

Energoelektronika

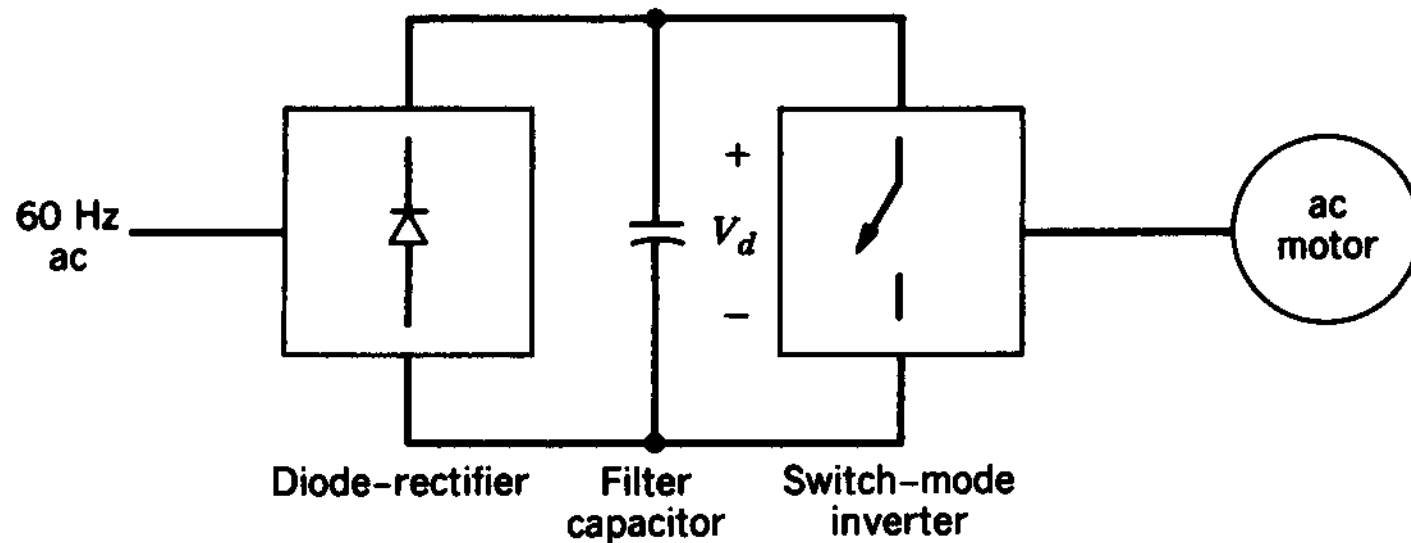
7. Switch-Mode DC- Sinusoidal AC Inverters

dr inż. Dariusz Janiszewski

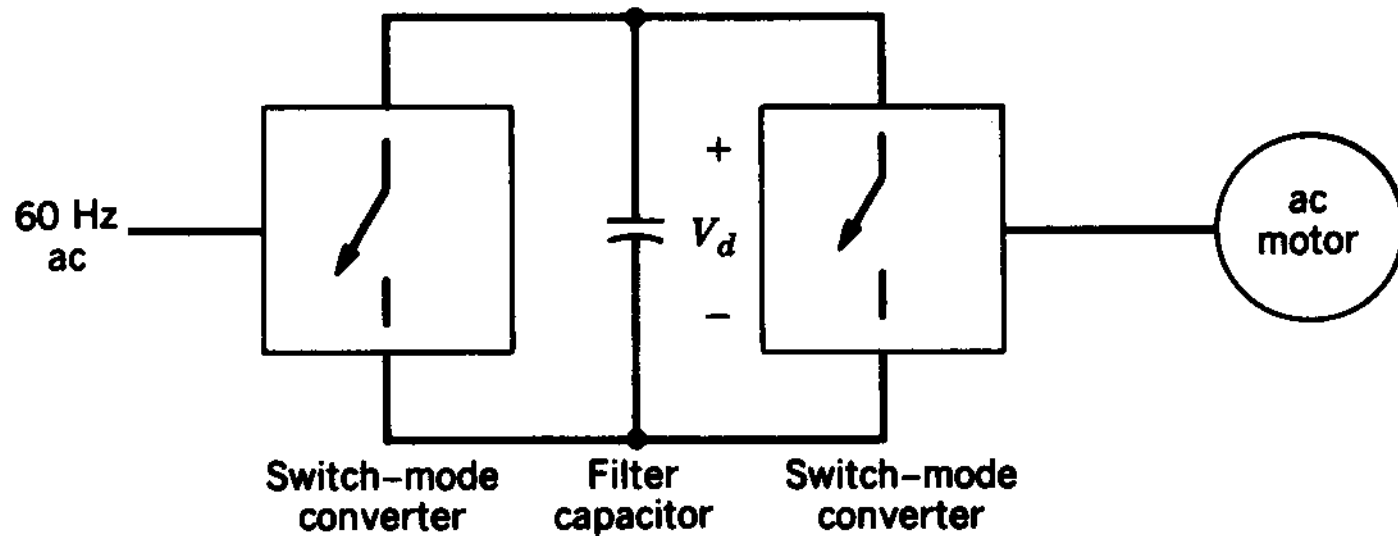
Plan

- ▶ Wprowadzenie do przetwornic DC-AC
- ▶ Koncepcja przetwornicy impulsowej – falownika
- ▶ Falownik jednofazowy
- ▶ Falownik trójfazowy
- ▶ Wpływ czasu martwego
- ▶ Inne falowniki
- ▶ Praca prostownikowa falownika

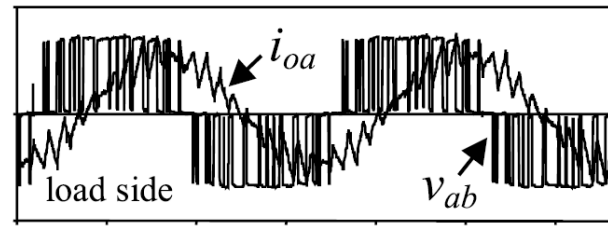
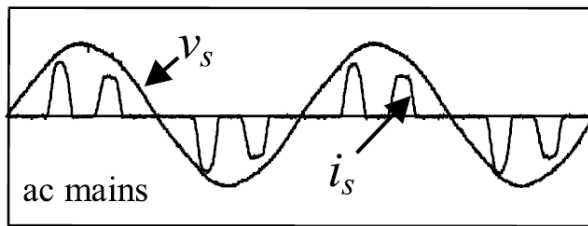
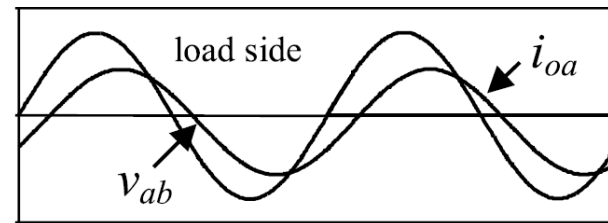
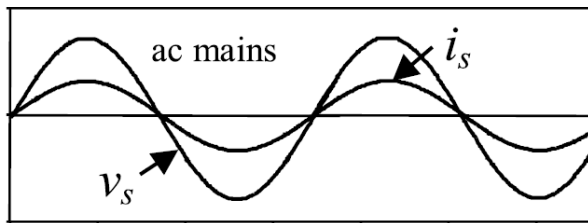
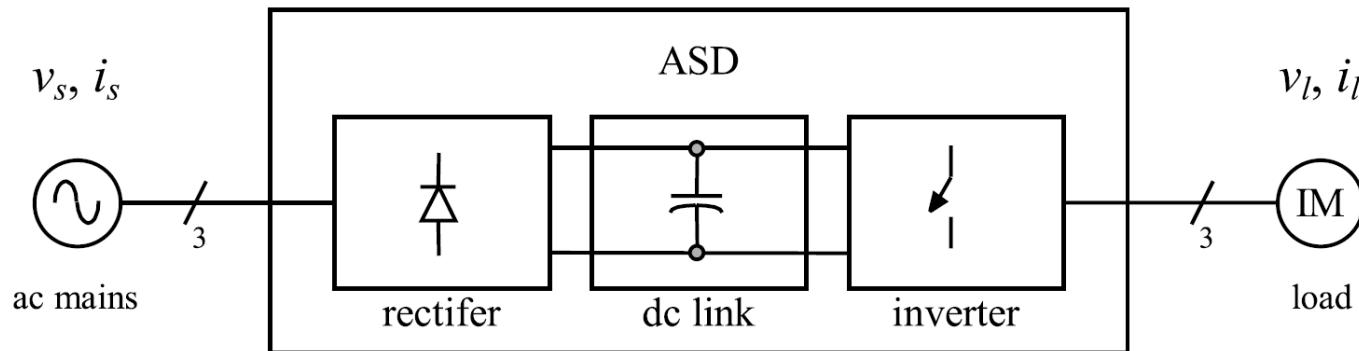
Switch-Mode DC-AC Inverter unidirectional



Switch-Mode DC-AC Inverter bidirectional

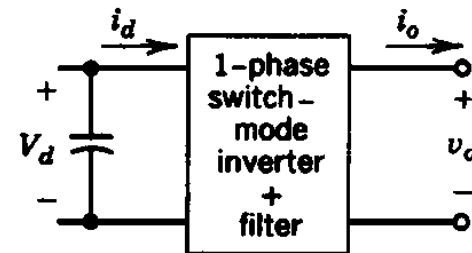
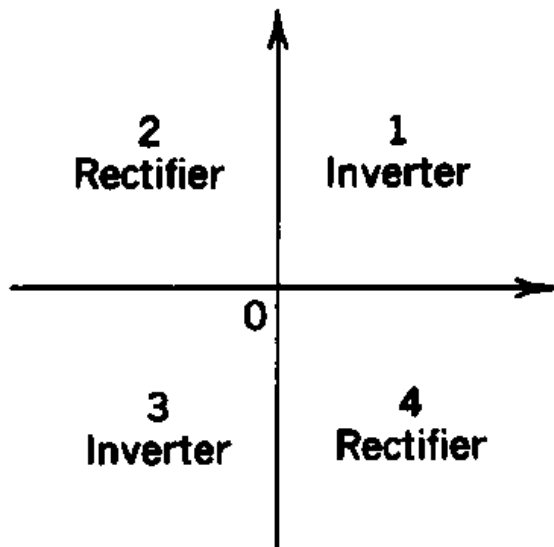


Standard adjustable speed drive scheme

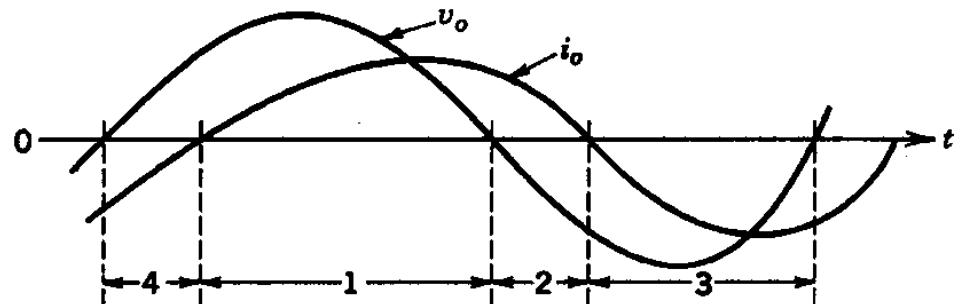


Switch-Mode DC-AC Inverter

► Four quadrants of operation



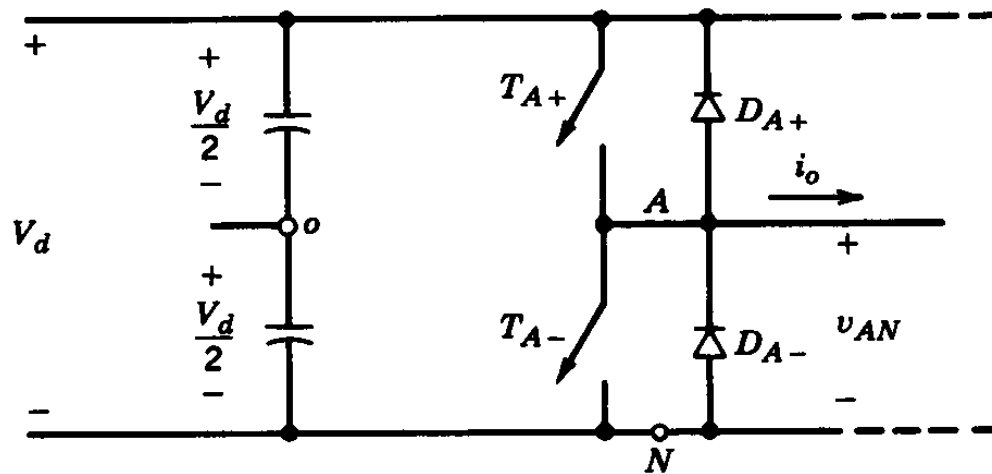
(a)



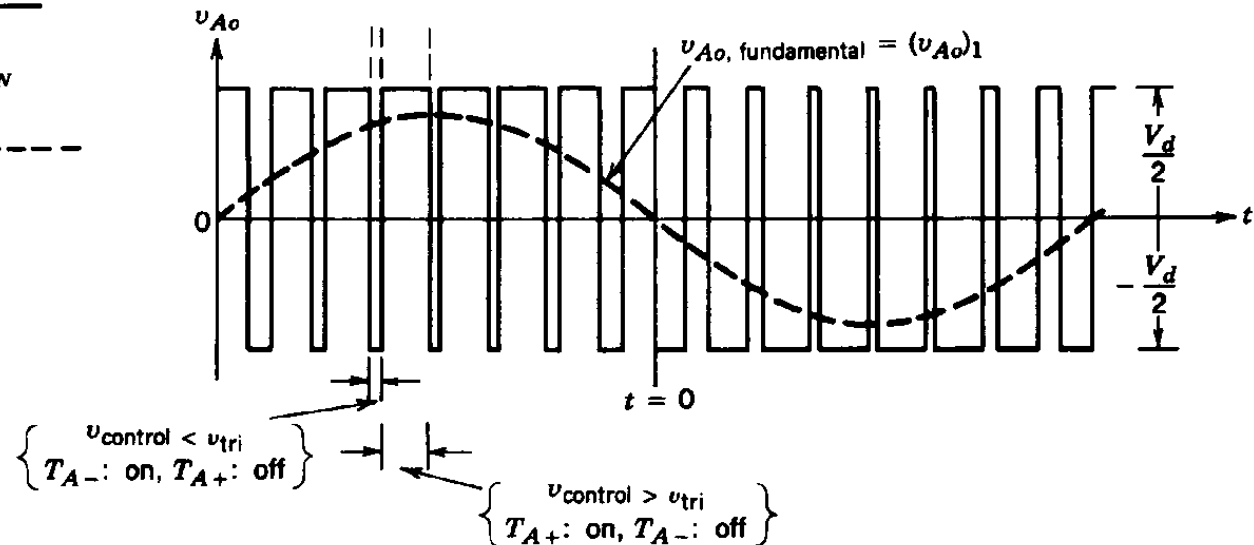
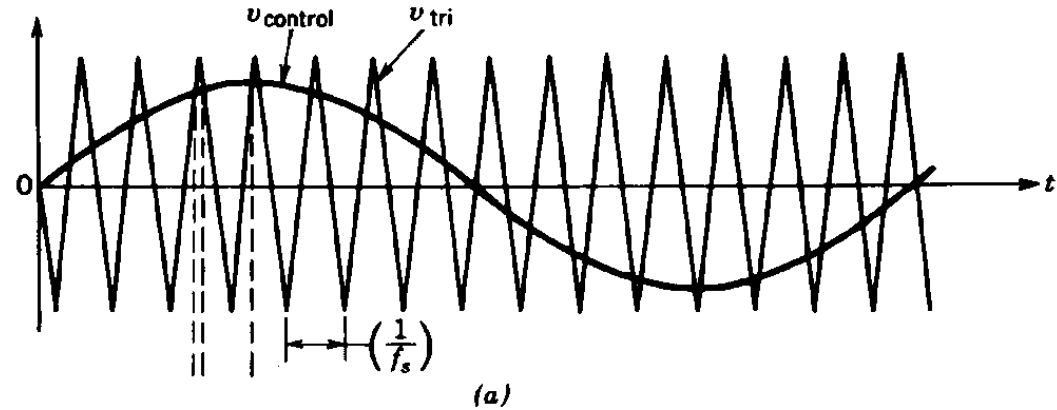
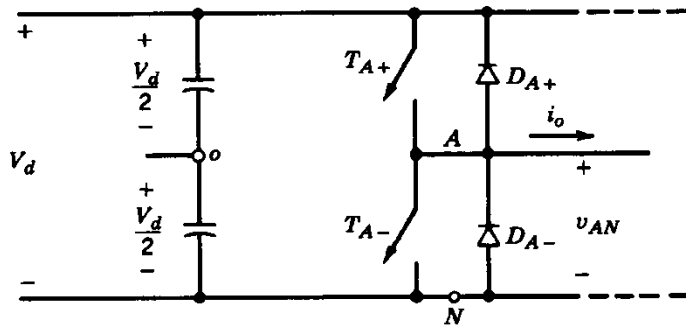
(b)

One Leg of a Switch-Mode DC-AC Inverter

- ▶ The mid-point shown is fictitious

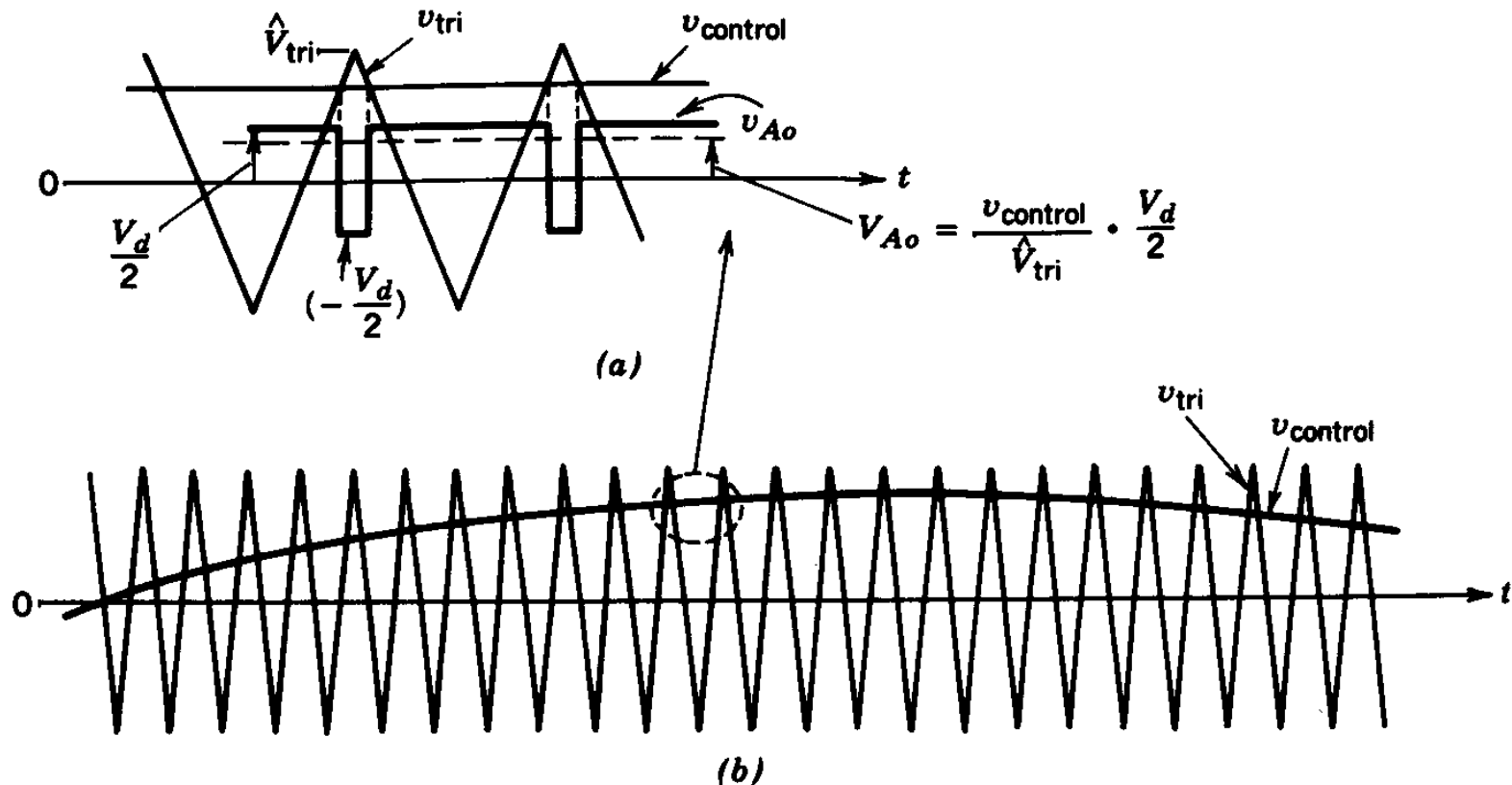


Synthesis of a Sinusoidal Output by PWM



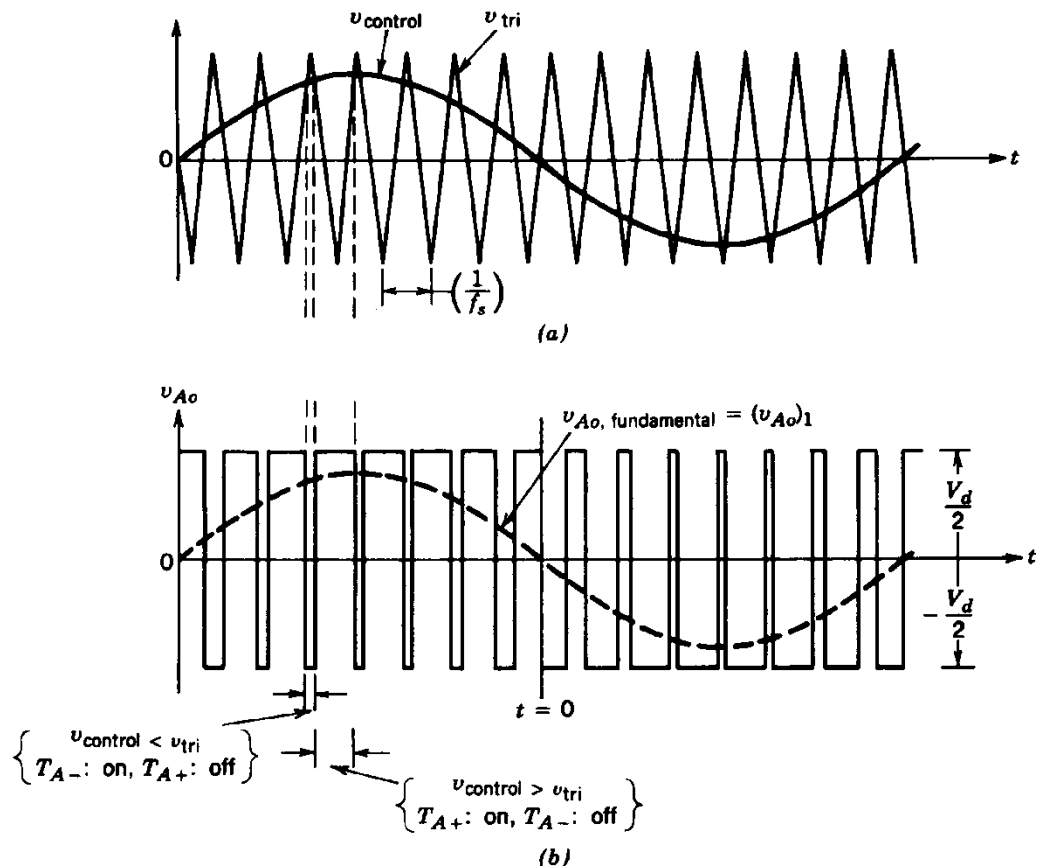
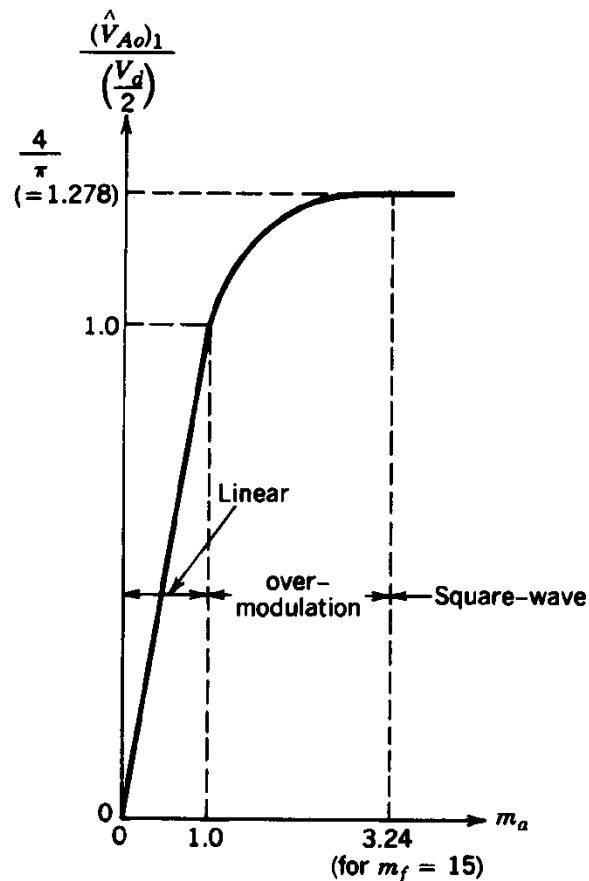
Details of a Switching Time Period

- Control voltage can be assumed constant during a switching time-period



Output voltage Fundamental as a Function of the Modulation Index

- Shows the linear and the over-modulation regions; square-wave operation in the limit



Harmonics in the DC-AC Inverter Output Voltage

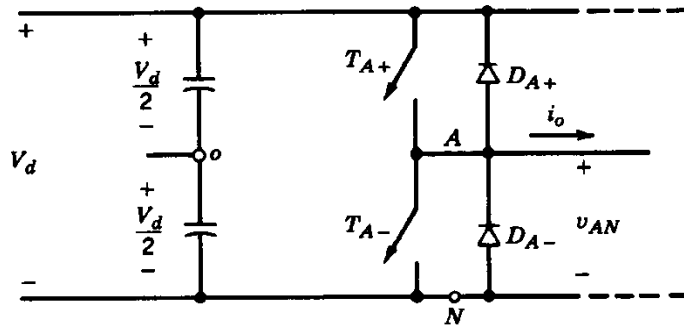
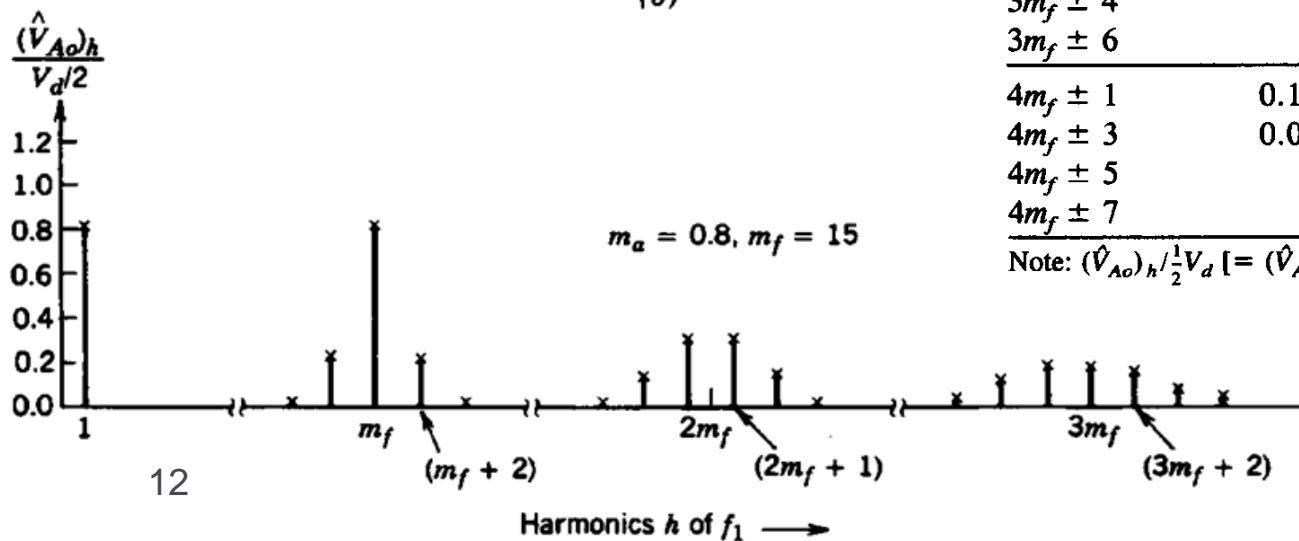


Table 8-1 Generalized Harmonics of v_{Ao} for a Large m_f .

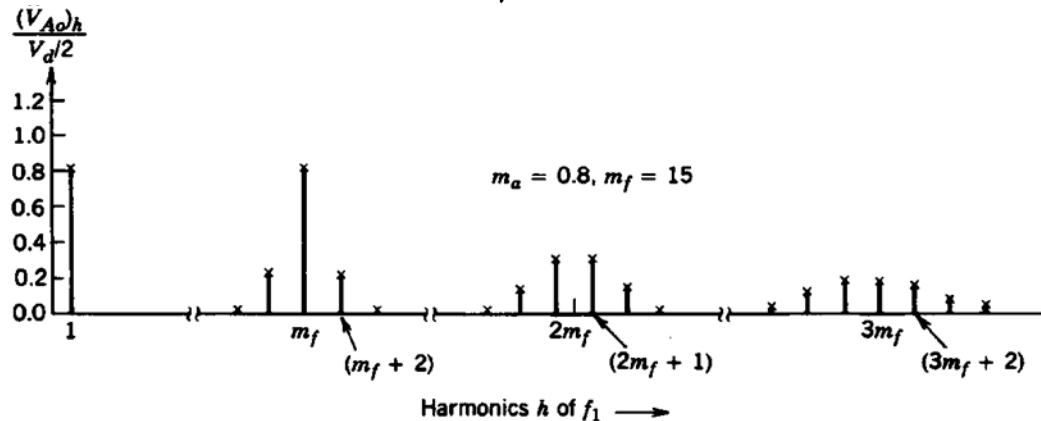
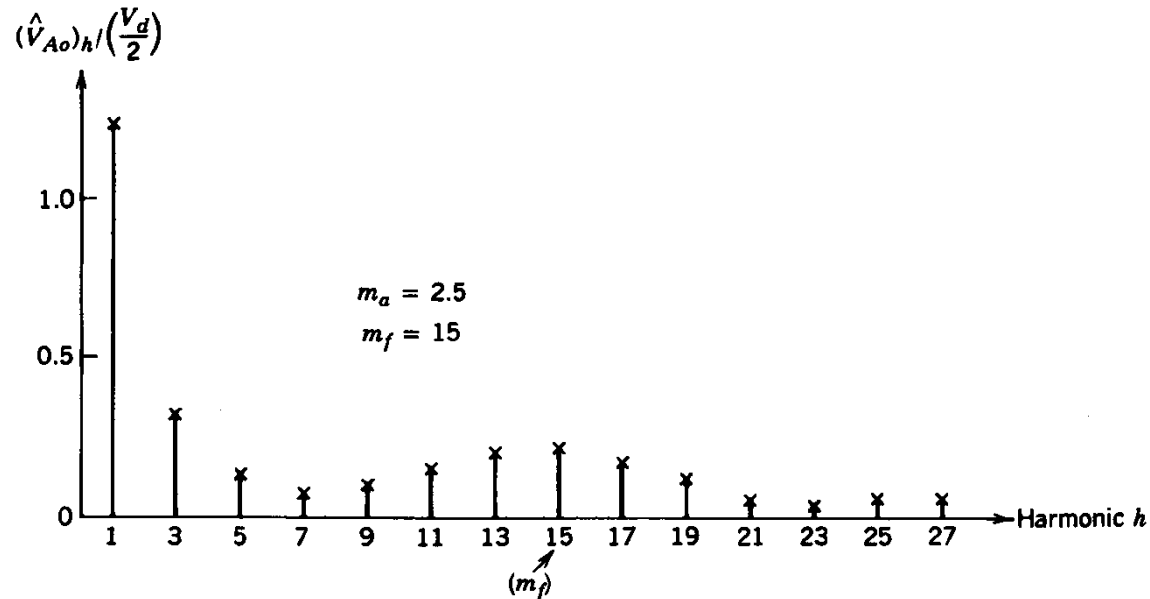
$h \backslash m_a$	0.2	0.4	0.6	0.8	1.0
1	0.2	0.4	0.6	0.8	1.0
<i>Fundamental</i>					
m_f	1.242	1.15	1.006	0.818	0.601
$m_f \pm 2$	0.016	0.061	0.131	0.220	0.318
$m_f \pm 4$					0.018
$2m_f \pm 1$	0.190	0.326	0.370	0.314	0.181
$2m_f \pm 3$		0.024	0.071	0.139	0.212
$2m_f \pm 5$				0.013	0.033
$3m_f$	0.335	0.123	0.083	0.171	0.113
$3m_f \pm 2$	0.044	0.139	0.203	0.176	0.062
$3m_f \pm 4$		0.012	0.047	0.104	0.157
$3m_f \pm 6$				0.016	0.044
$4m_f \pm 1$	0.163	0.157	0.008	0.105	0.068
$4m_f \pm 3$	0.012	0.070	0.132	0.115	0.009
$4m_f \pm 5$			0.034	0.084	0.119
$4m_f \pm 7$				0.017	0.050

Note: $(\hat{V}_{Ao})_h / \frac{1}{2}V_d [= (\hat{V}_{AN})_h / \frac{1}{2}V_d]$ is tabulated as a function of m_a .



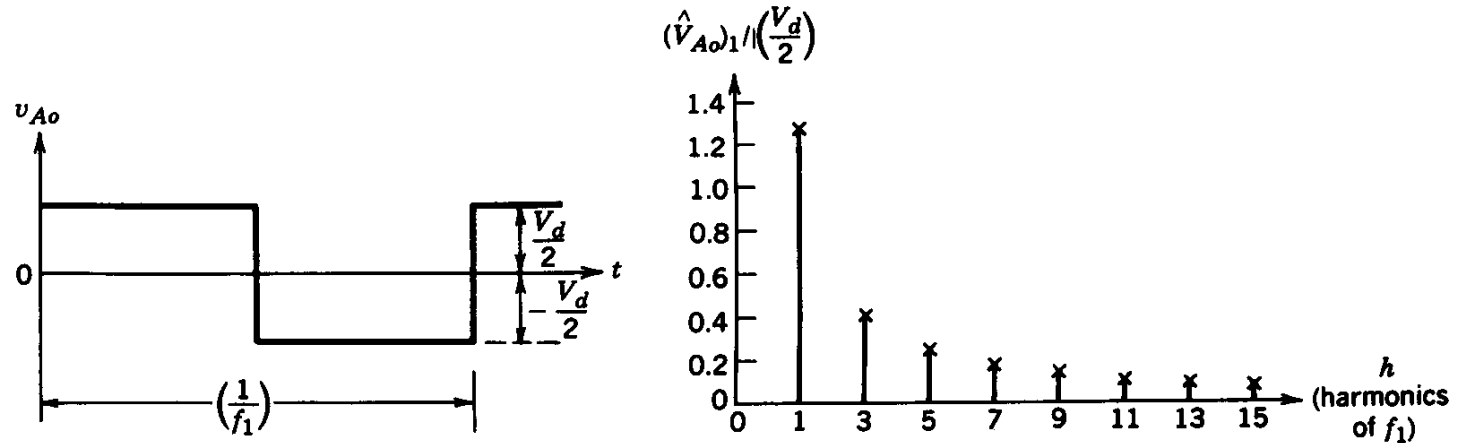
Harmonics due to Over-modulation

- These are harmonics of the fundamental frequency



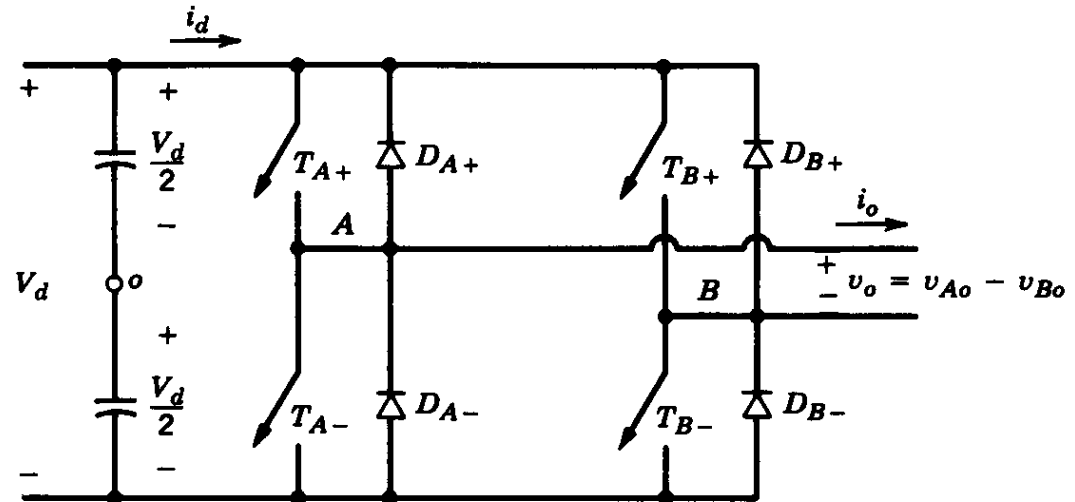
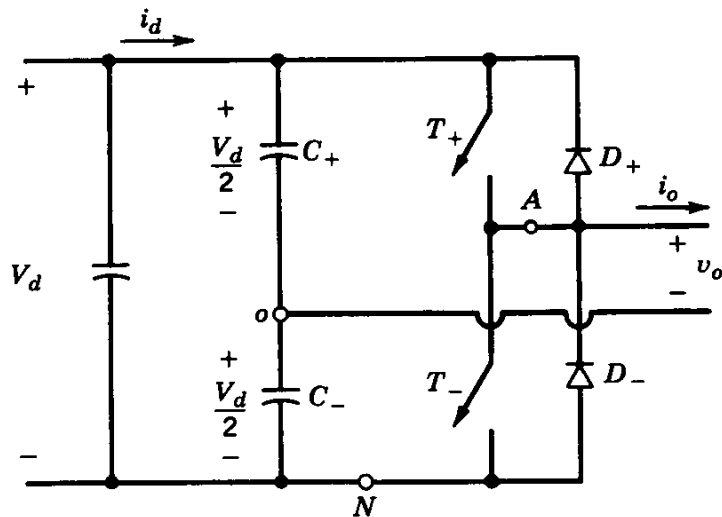
Square-Wave Mode of Operation

- ▶ Harmonics are of the fundamental frequency

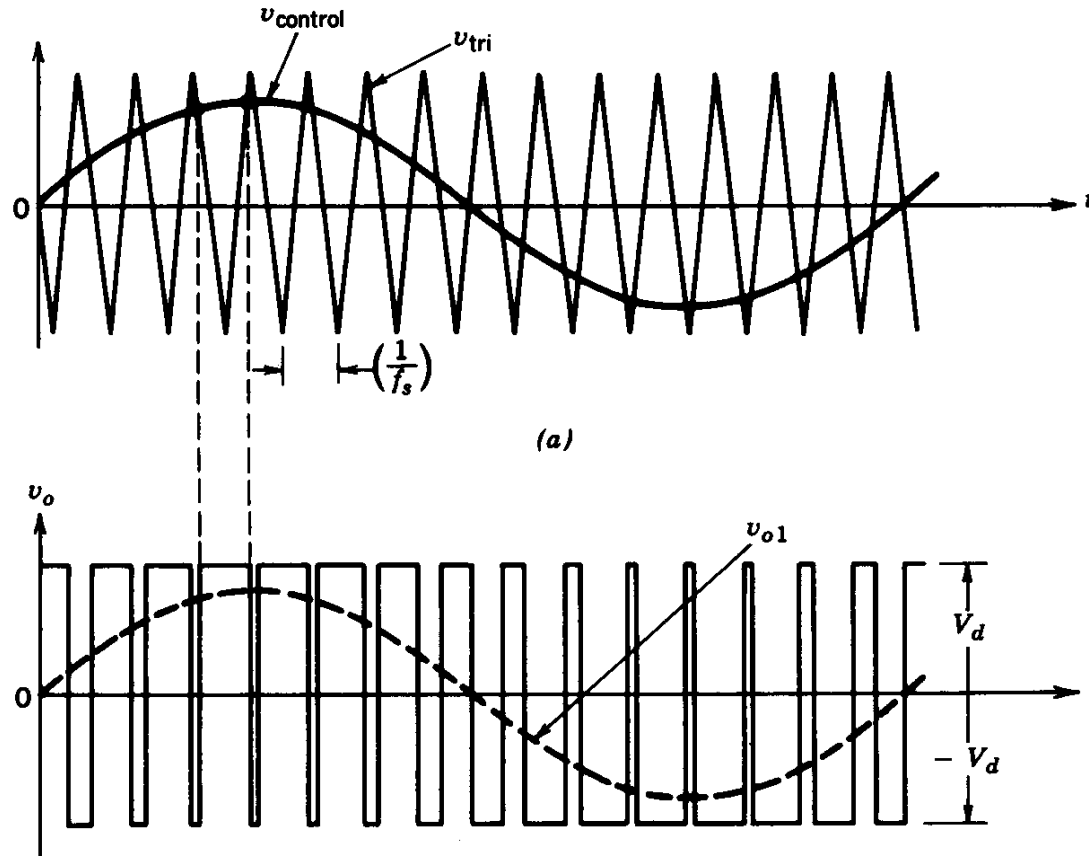


Half-Bridge / Full-Bridge Inverter

- ▶ Capacitors provide the mid-point
- ▶ Consists of two inverter legs



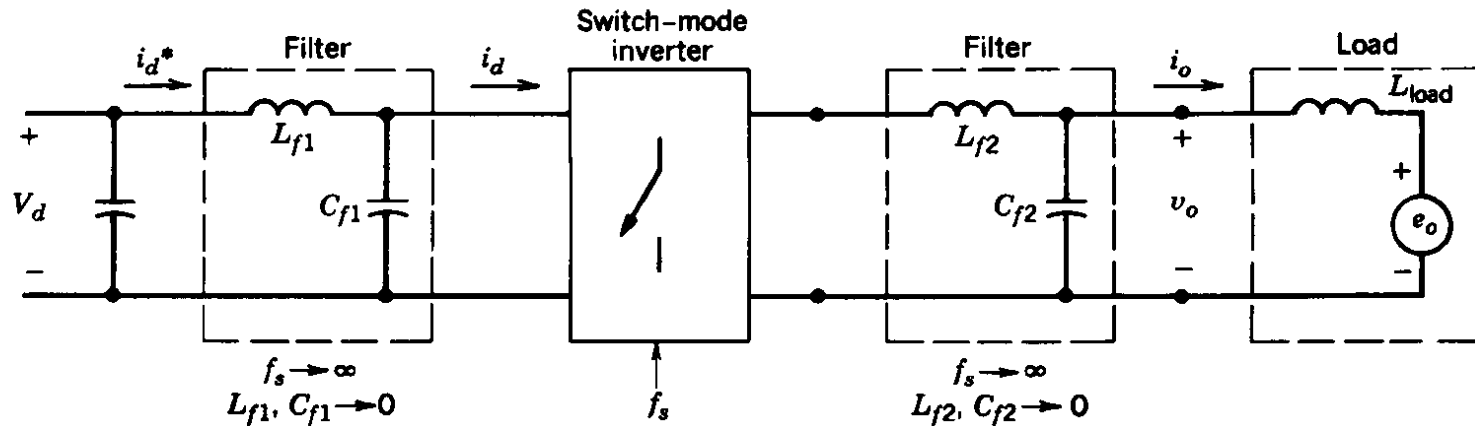
PWM to Synthesize Sinusoidal Output



- ▶ The dotted curve is the desired output; also the fundamental frequency
- ▶ Bipolar voltage switching

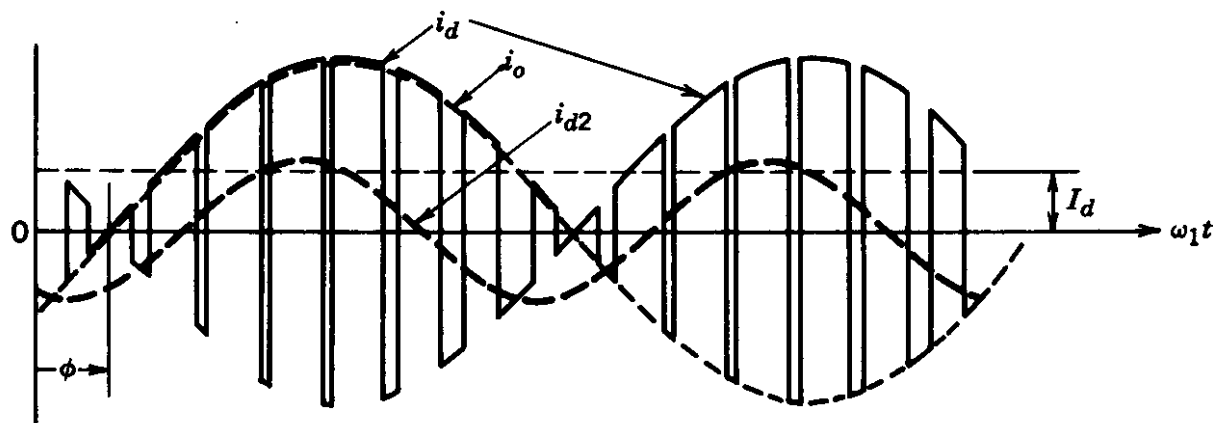
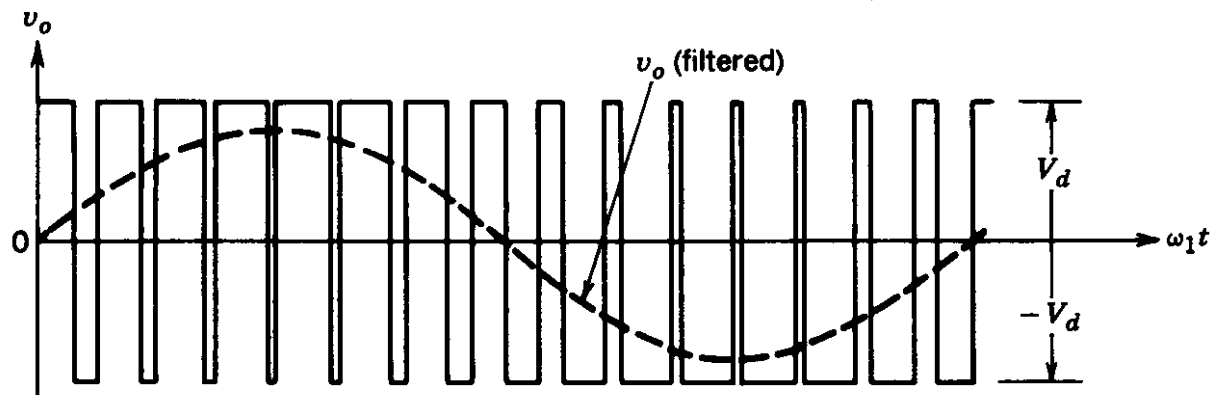
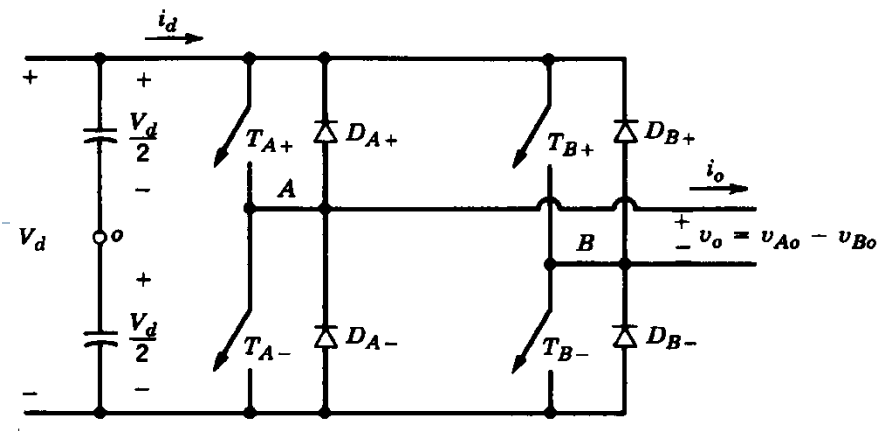
Analysis assuming Fictitious Filters

- ▶ Small fictitious filters eliminate the switching-frequency related ripple

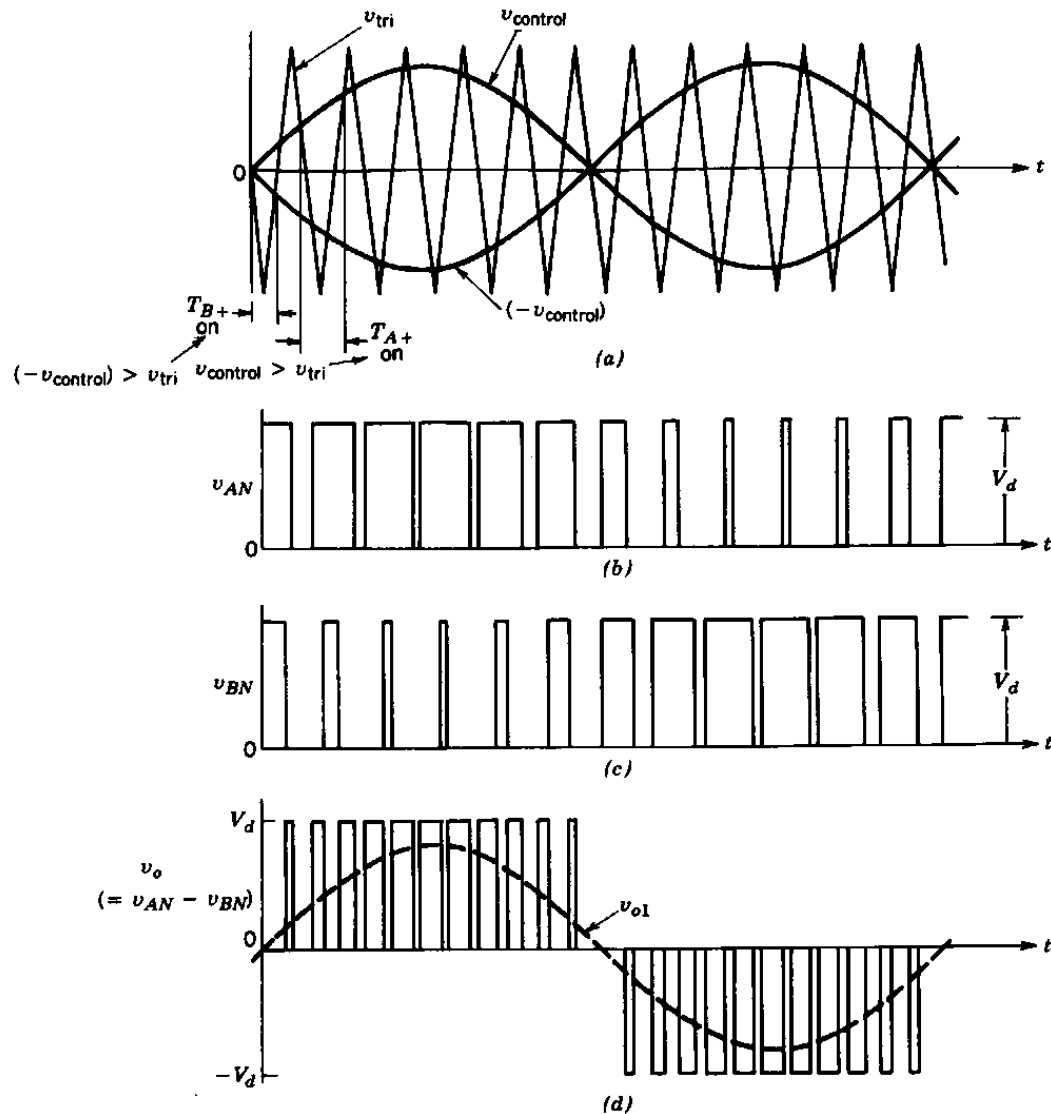


DC-Side Current

► Bi-Polar Voltage switching

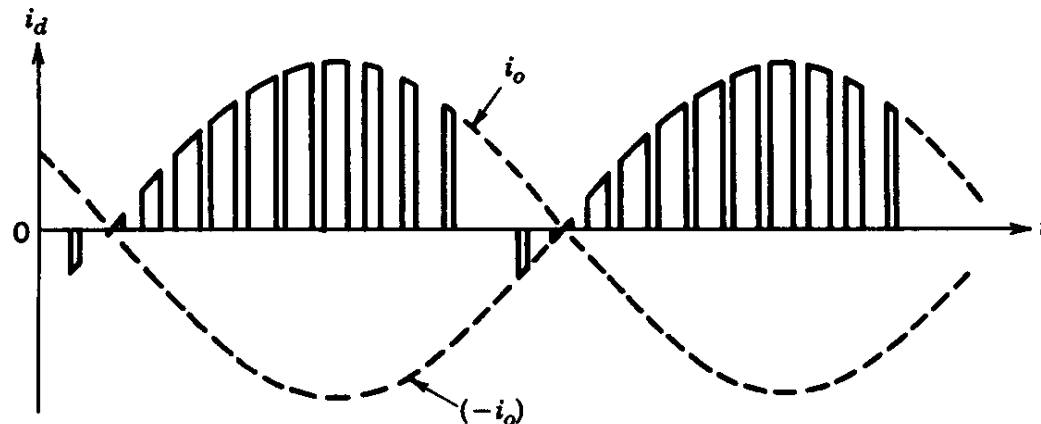
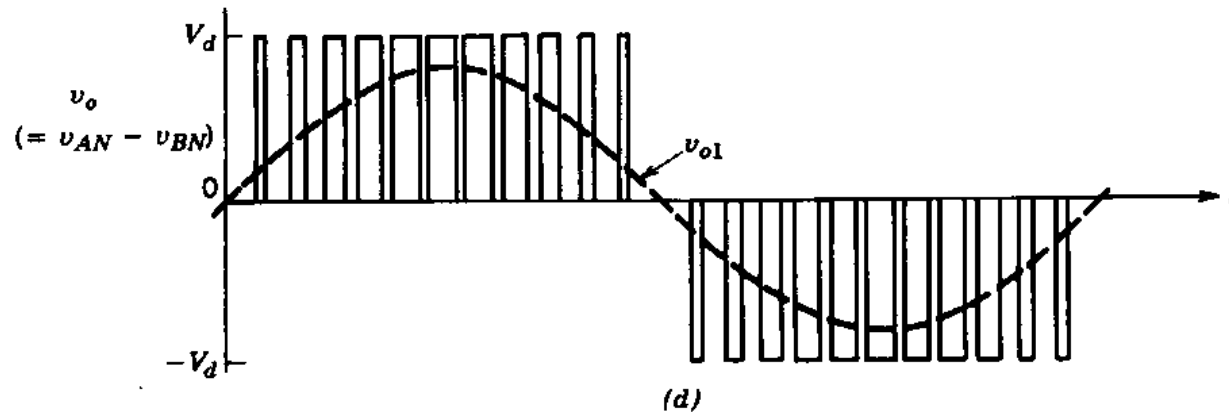


Output Waveforms: Uni-polar Voltage Switching

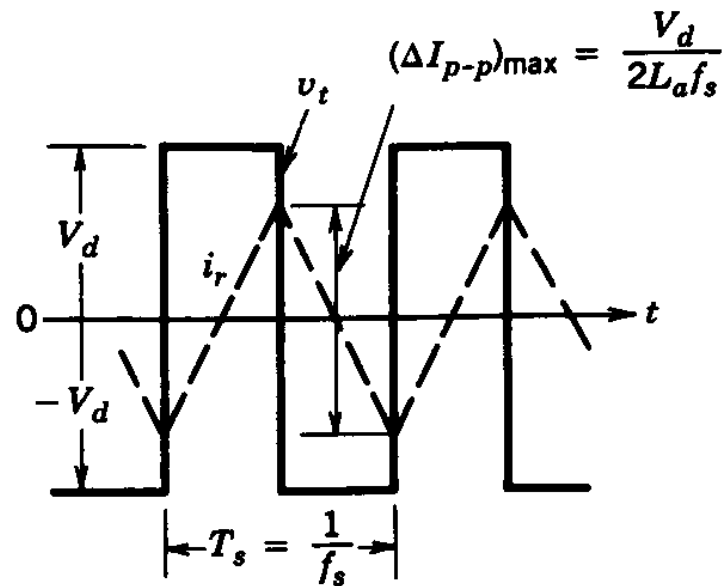


DC-Side Current in a Single-Phase Inverter

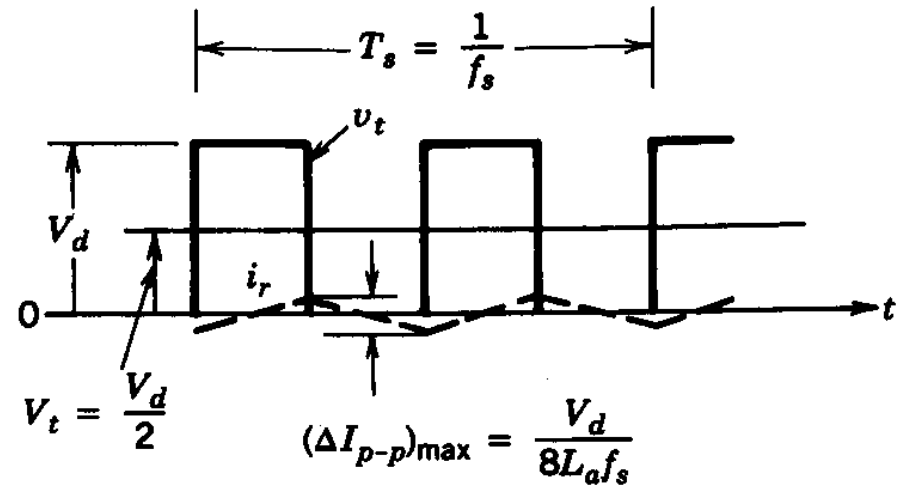
- Uni-polar voltage switching



Bipolar and Unipolar Current Ripple



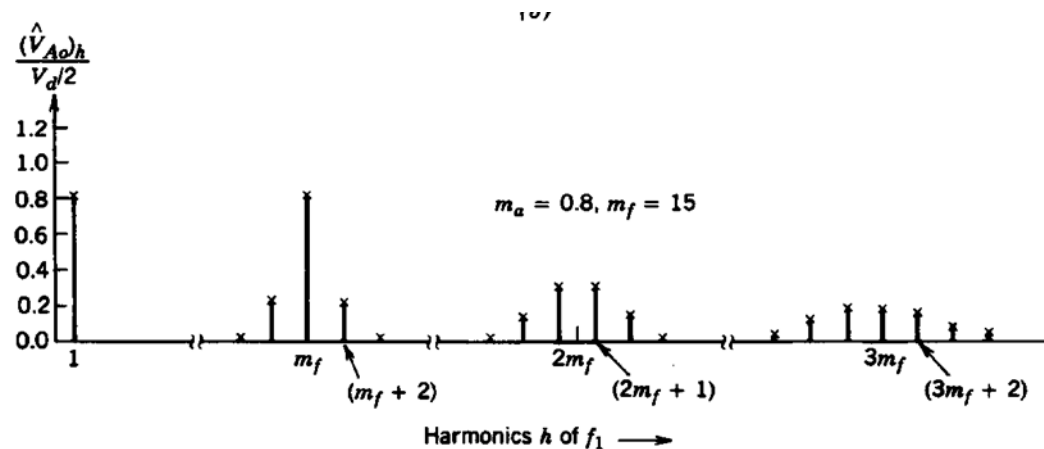
(a)



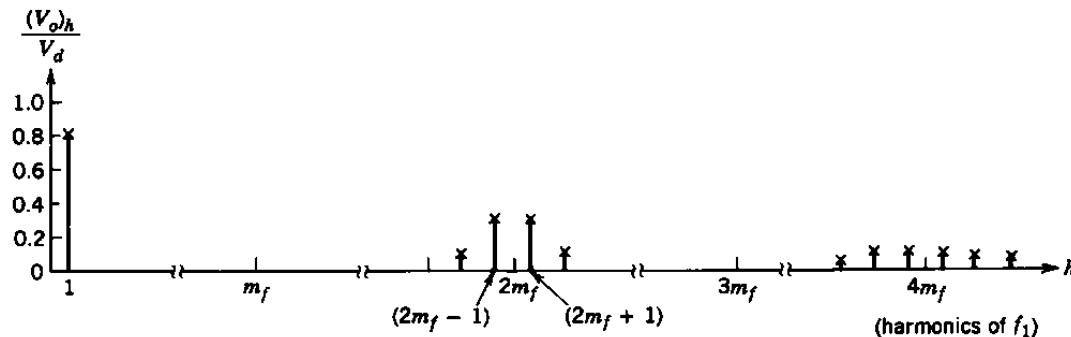
(b)

Harmonic Components during Bi-polar / Uni-polar Voltage Switching

► Bi-Polar



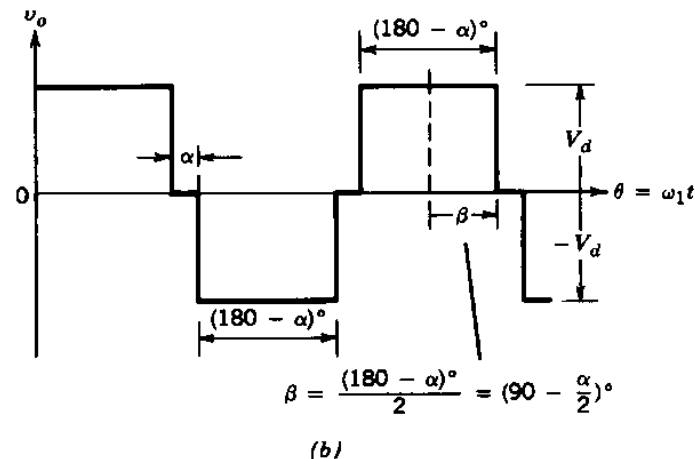
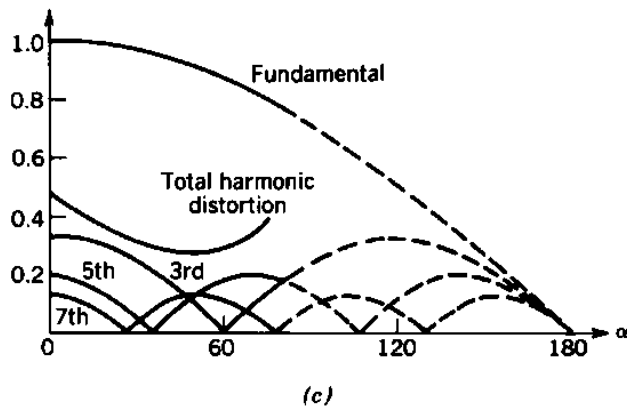
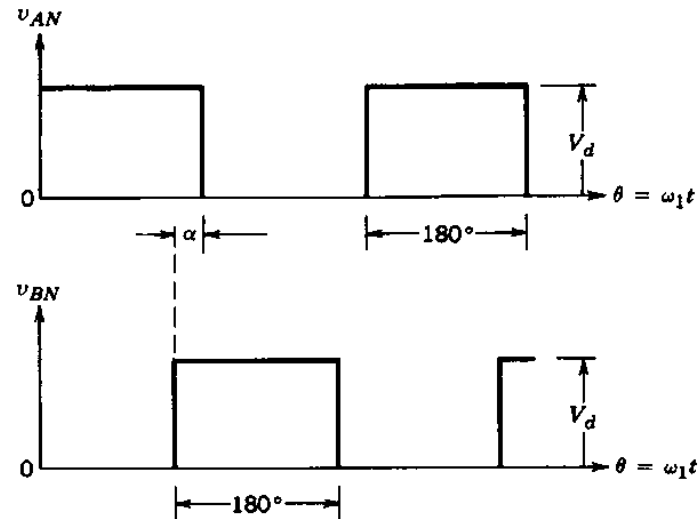
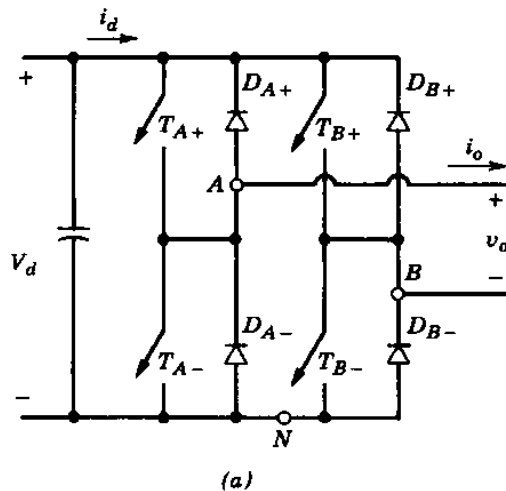
► Uni-Polar



- Harmonic components around the switching frequency are absent in UP!

Sinusoidal Synthesis by Voltage Shift

- Phase shift allows voltage cancellation to synthesize a 1-Phase sinusoidal output

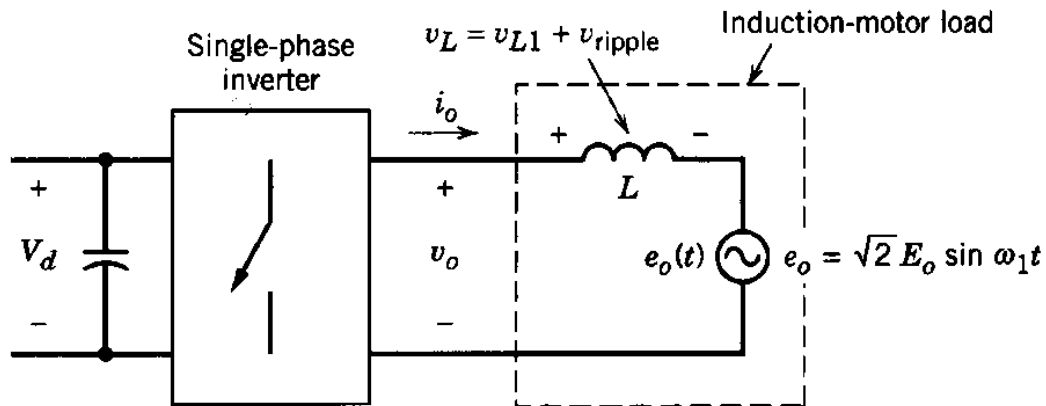


$$\beta = \frac{(180 - \alpha)^\circ}{2} = (90 - \frac{\alpha}{2})^\circ$$

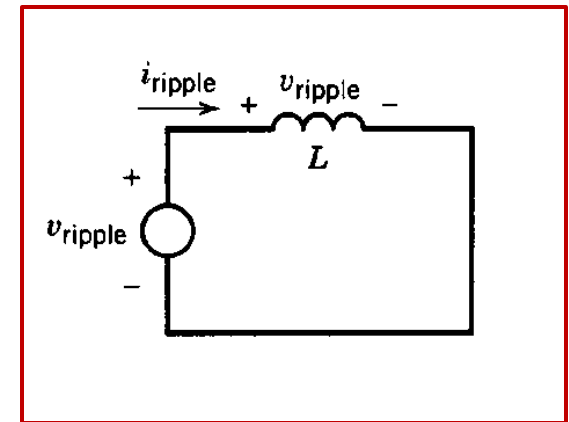
Voltage Ripple

Single-Phase Inverter

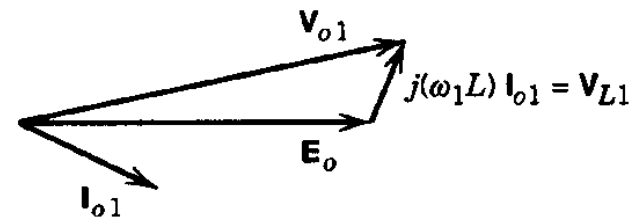
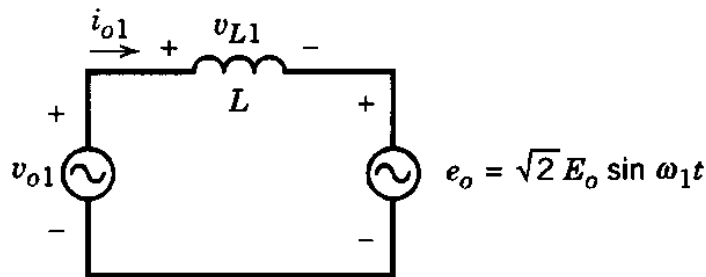
► Analysis at the fundamental frequency



(a)



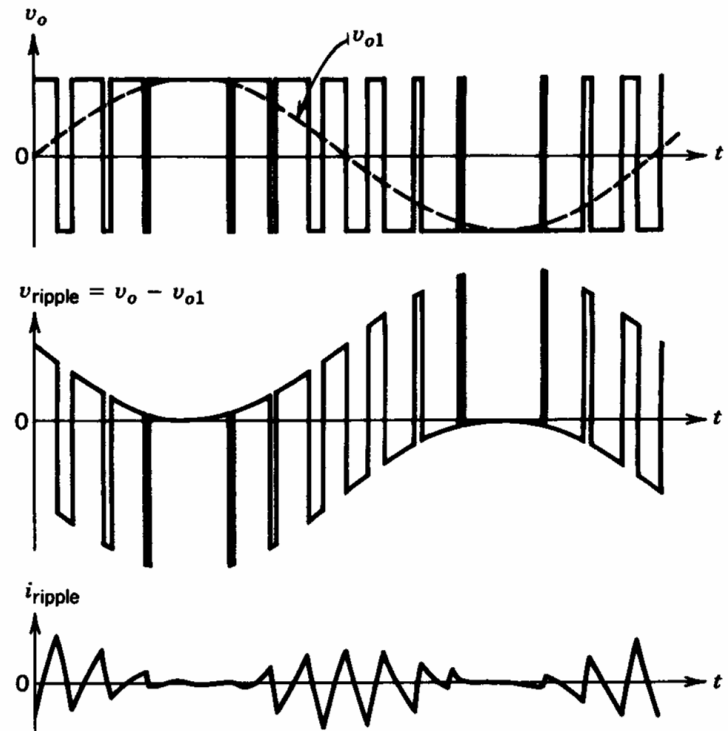
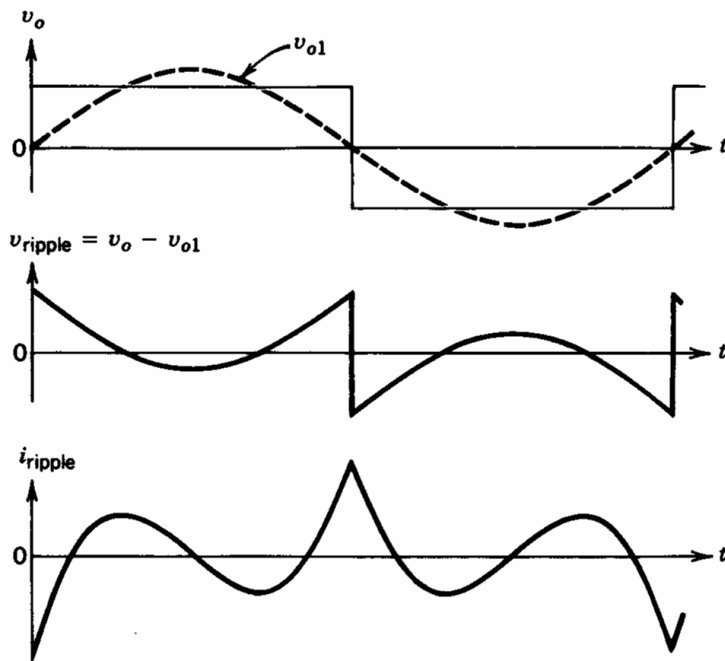
(c)



Voltage/Current Ripple

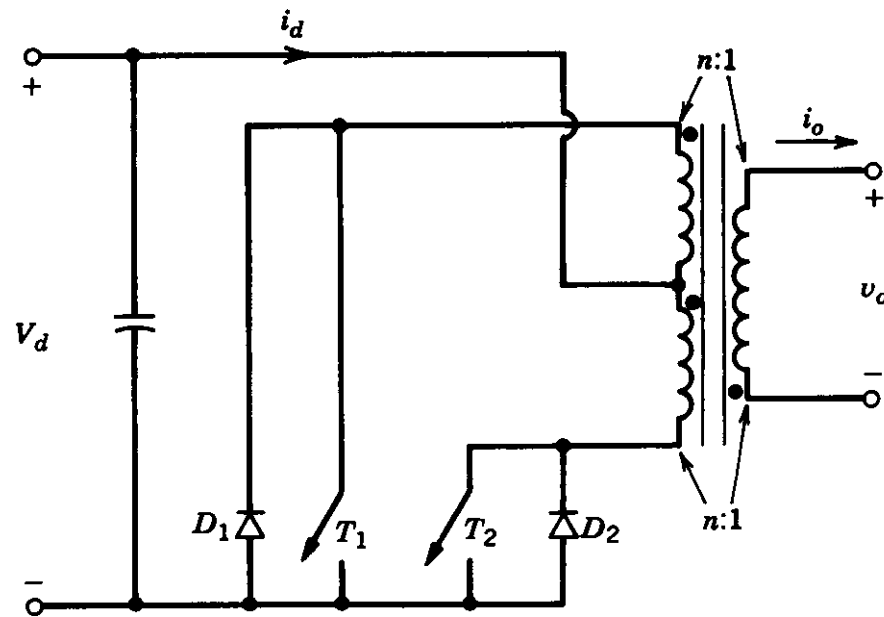
Square-Wave and PWM Operation

- ▶ PWM results in much smaller ripple current



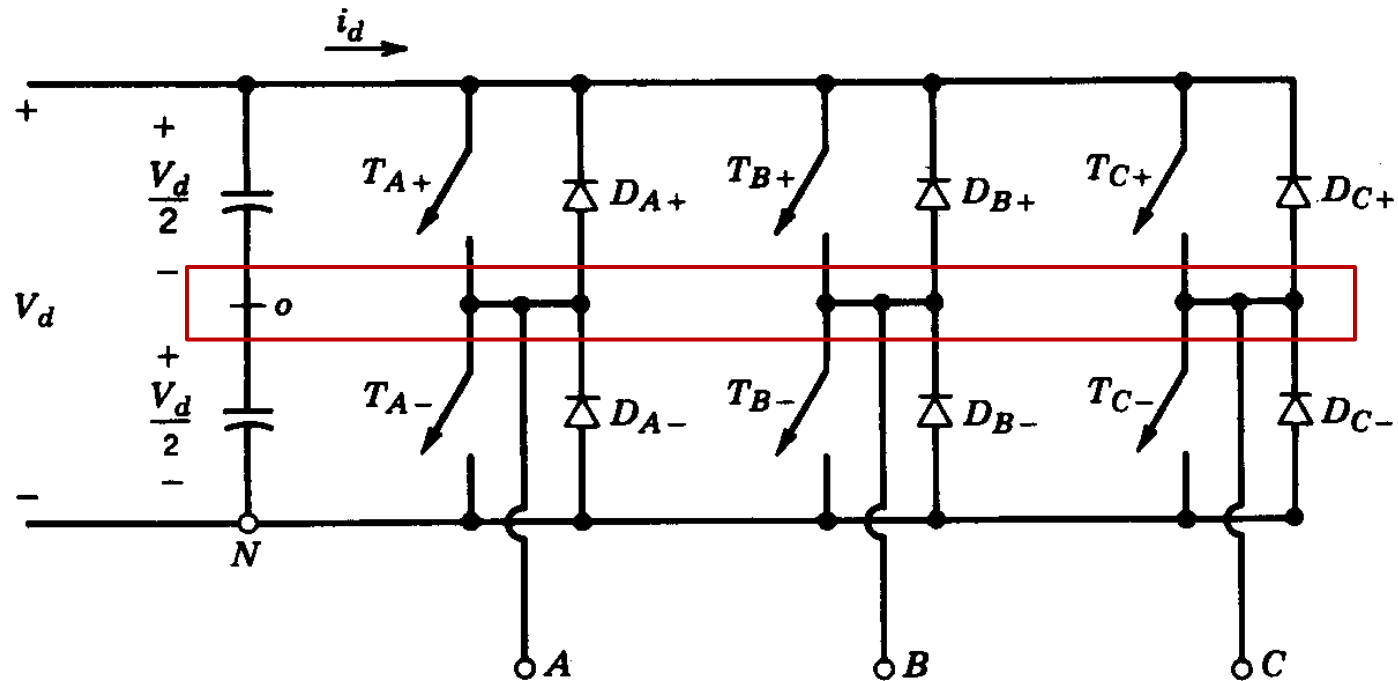
Push-Pull Inverter

- ▶ Low Voltage to higher output using square-wave operation

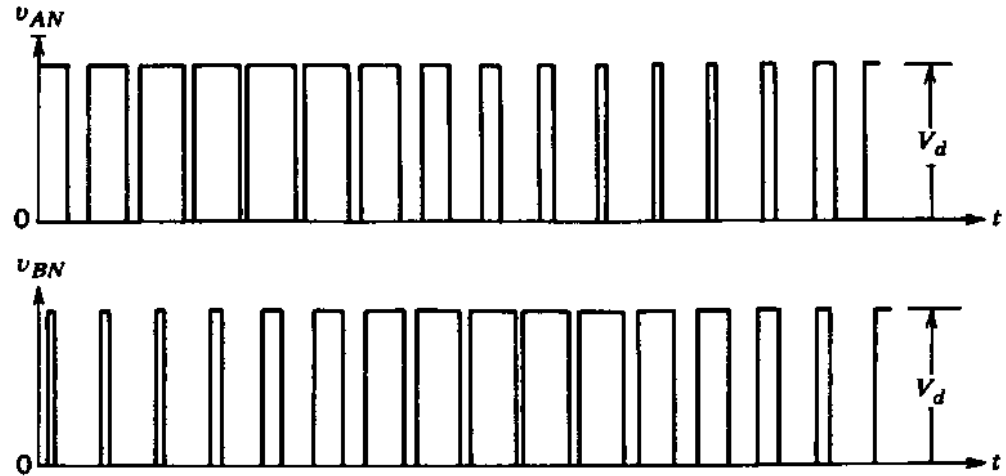
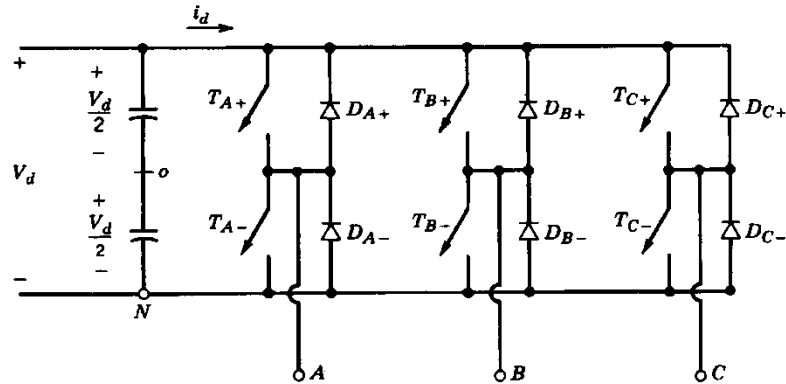
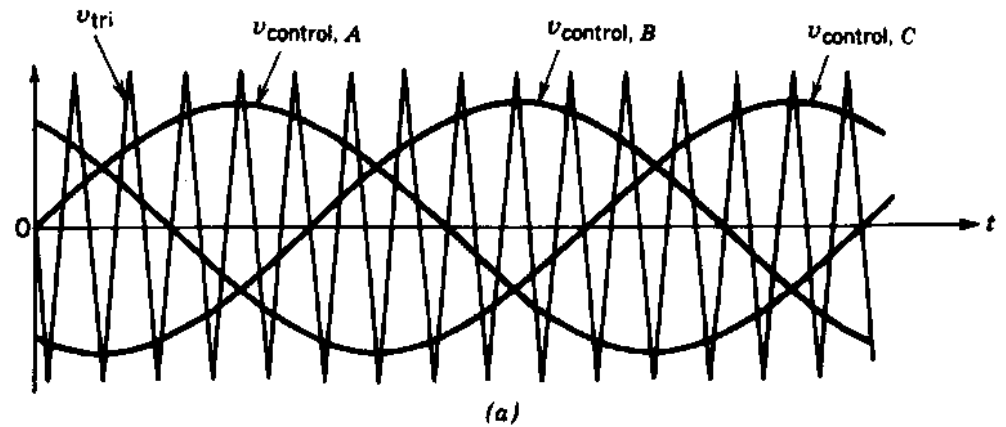


Three-Phase Inverter

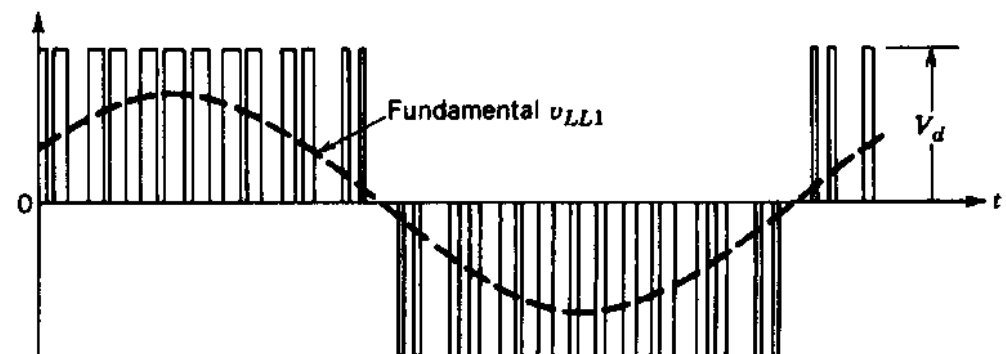
- Three inverter legs; capacitor mid-point is fictitious



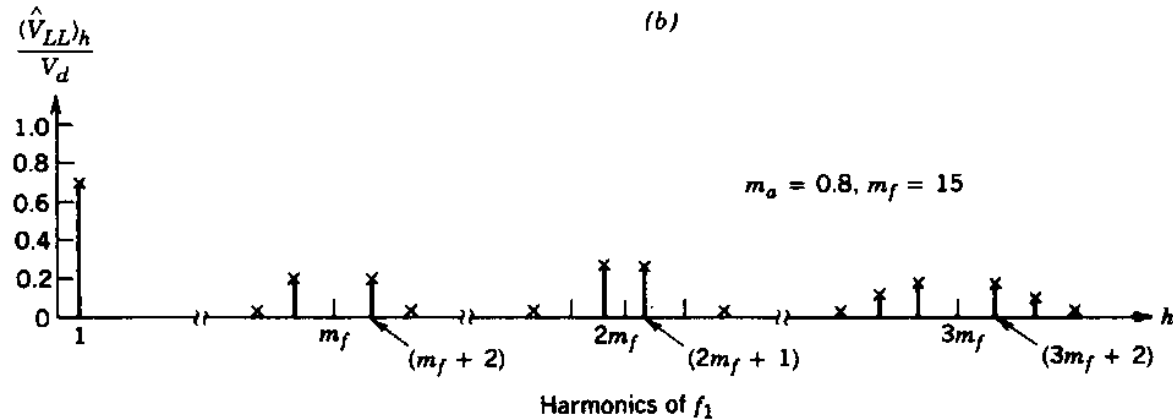
Three-Phase PWM Waveforms



$$v_{AB} = v_{AN} - v_{BN}$$



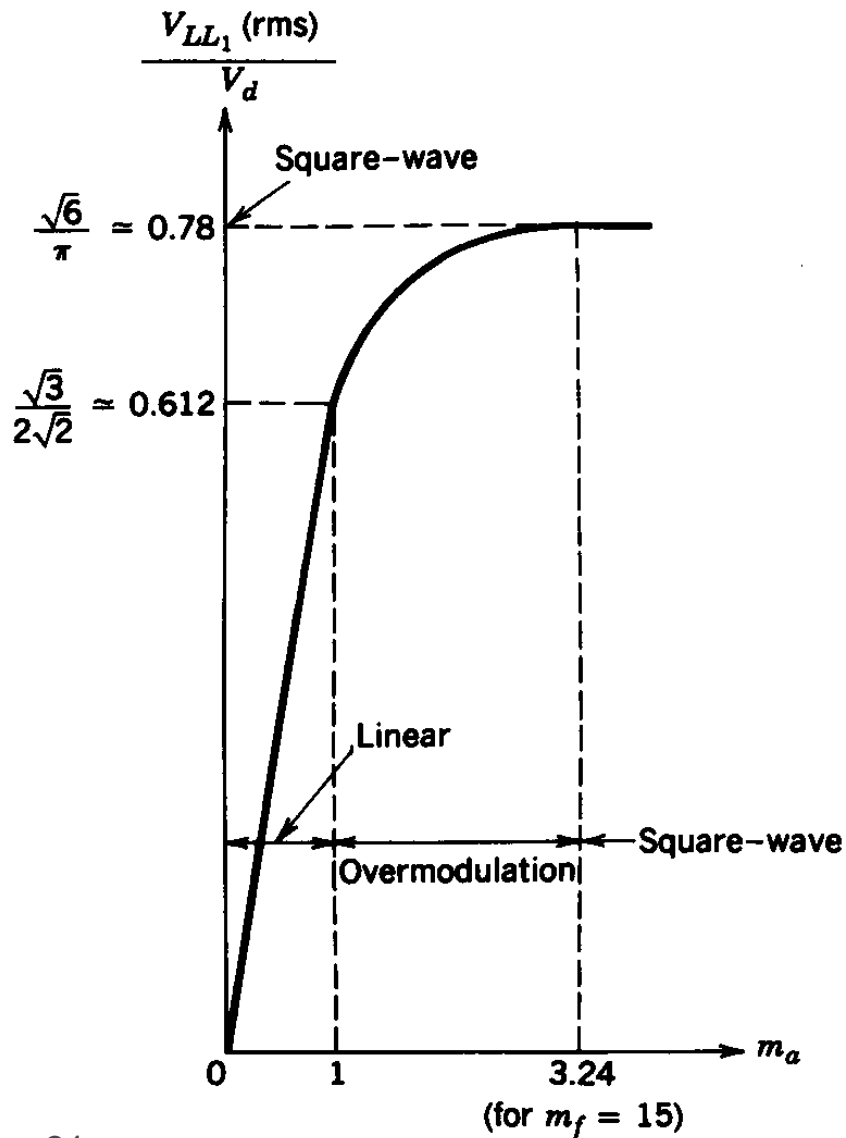
Three-Phase Inverter Harmonics



$h \backslash m_a$	0.2	0.4	0.6	0.8	1.0
1	0.122	0.245	0.367	0.490	0.612
$m_f \pm 2$	0.010	0.037	0.080	0.135	0.195
$m_f \pm 4$				0.005	0.011
$2m_f \pm 1$	0.116	0.200	0.227	0.192	0.111
$2m_f \pm 5$				0.008	0.020
$3m_f \pm 2$	0.027	0.085	0.124	0.108	0.038
$3m_f \pm 4$		0.007	0.029	0.064	0.096
$4m_f \pm 1$	0.100	0.096	0.005	0.064	0.042
$4m_f \pm 5$			0.021	0.051	0.073
$4m_f \pm 7$				0.010	0.030

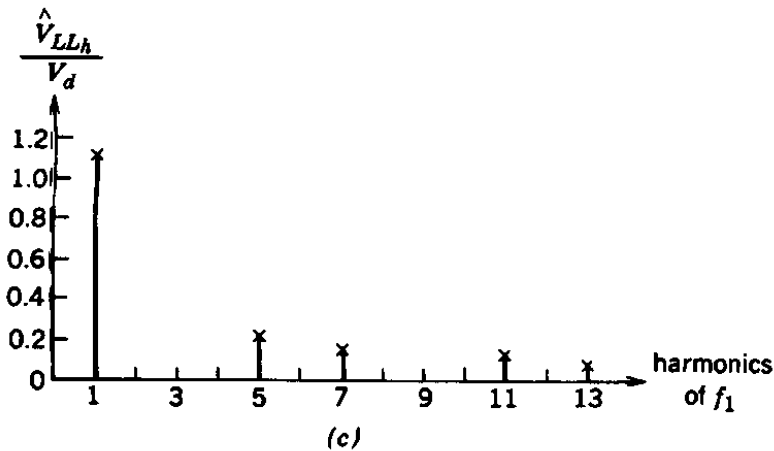
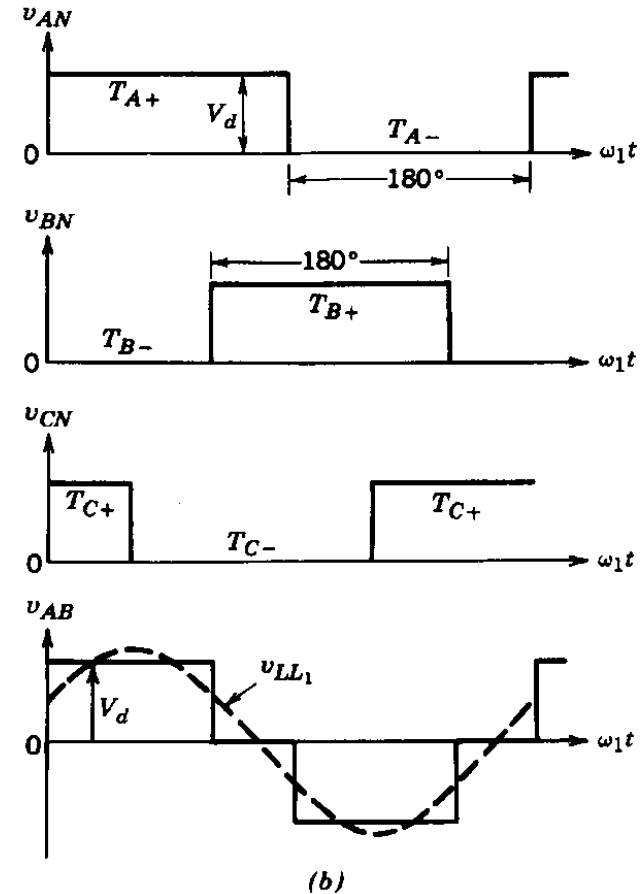
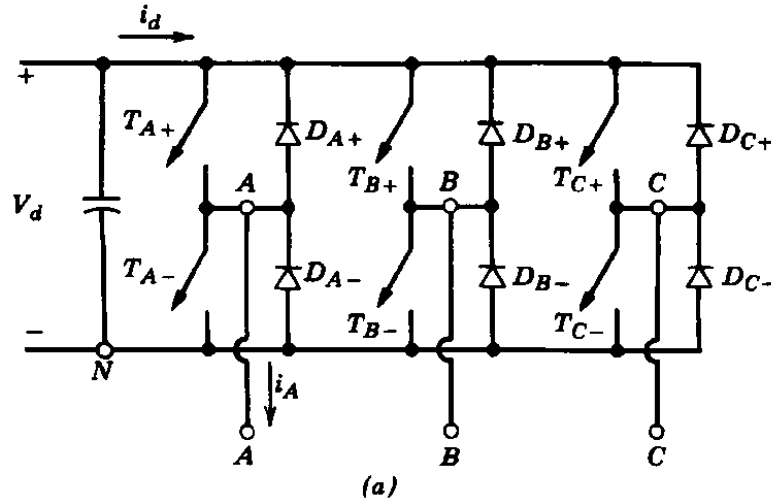
Note: $(V_{LL})_h/V_d$ are tabulated as a function of m_a where $(V_{LL})_h$ are the rms values of the harmonic voltages.

Three-Phase Inverter Output



- ▶ Linear
- ▶ over-modulation ranges

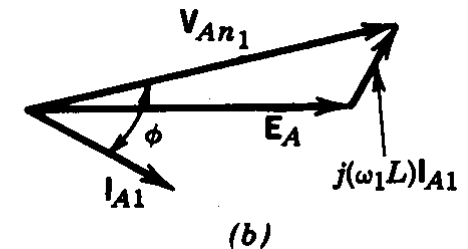
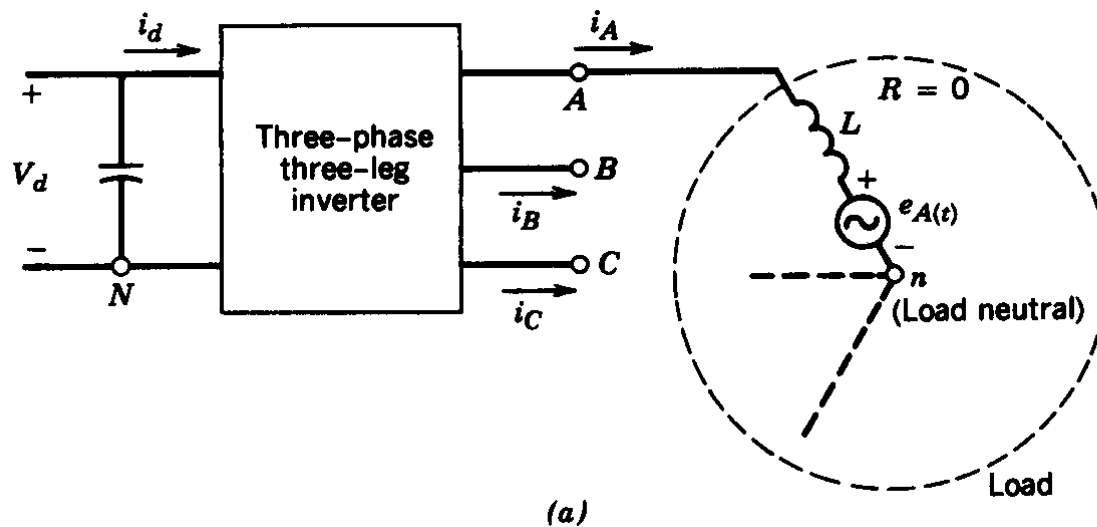
Three-Phase Inverter: Square-Wave Mode



- Harmonics are of the fundamental frequency

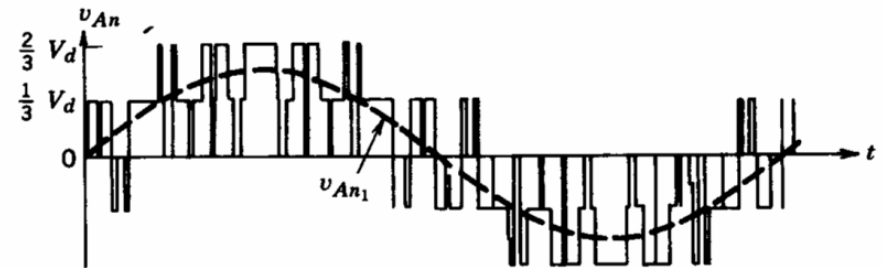
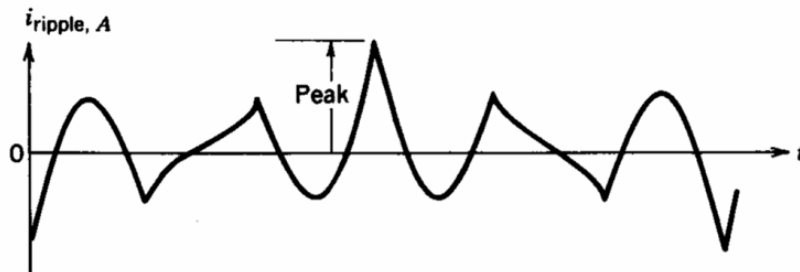
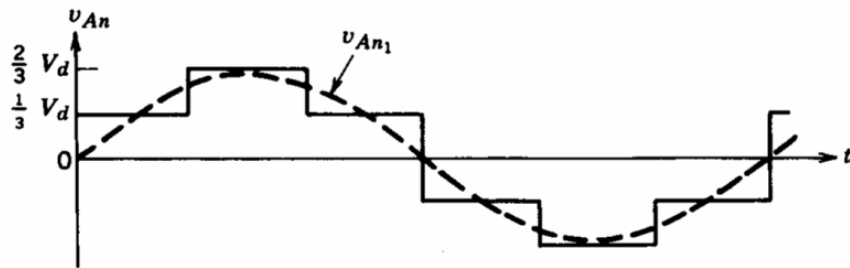
Three-Phase Inverter: Fundamental Frequency

- ▶ Analysis at the fundamental frequency can be done using phasors



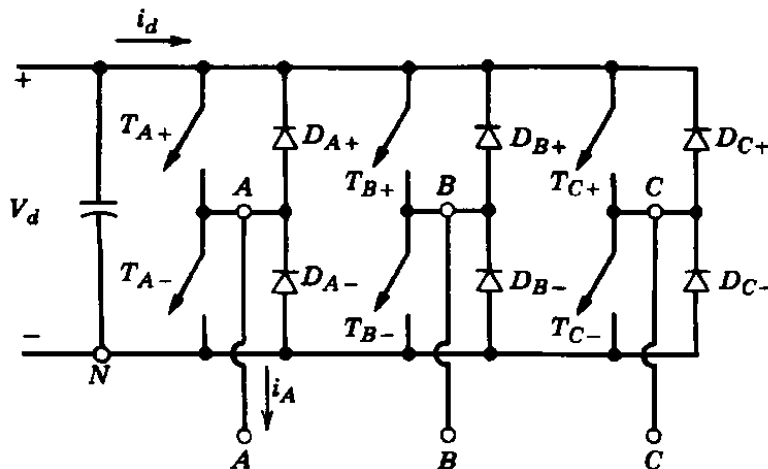
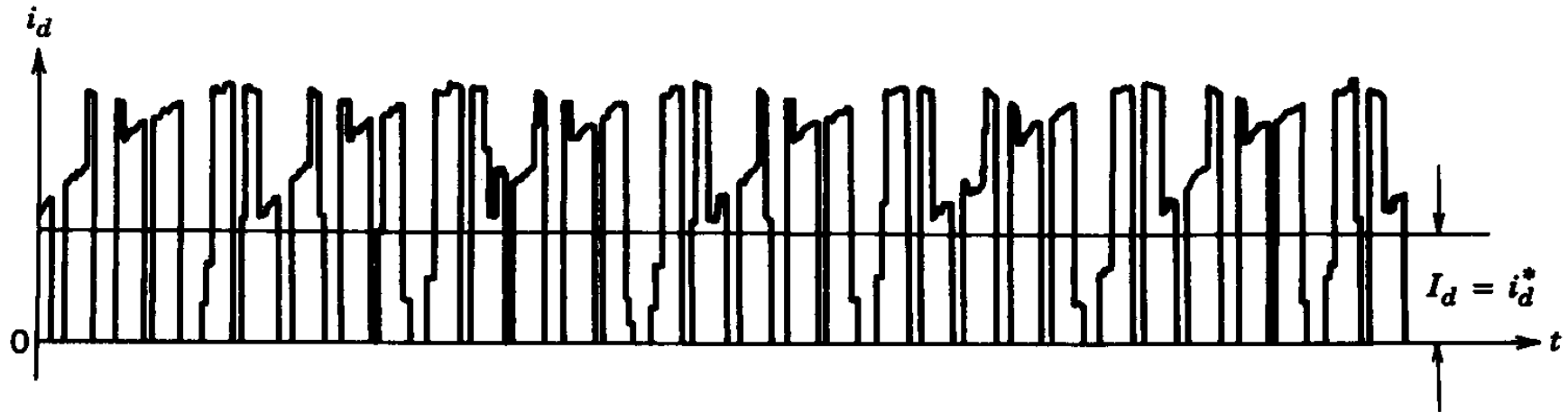
Voltage and Current Ripple

Square-Wave and PWM Operation



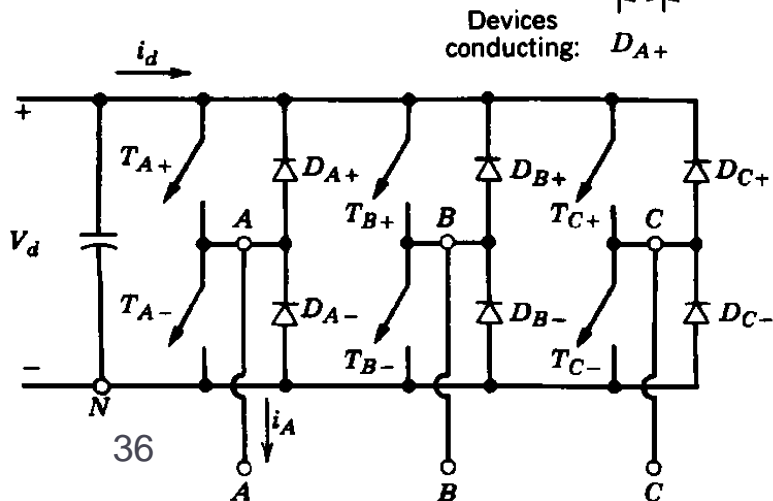
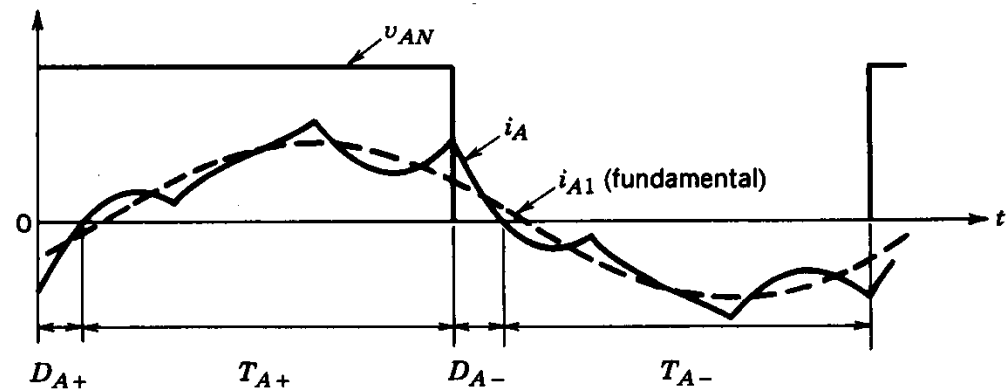
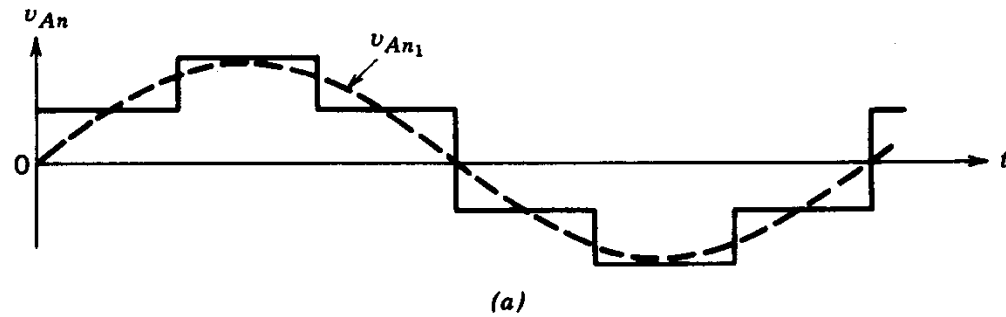
- PWM results in much smaller ripple current

DC-Side Current in a Three-Phase Inverter

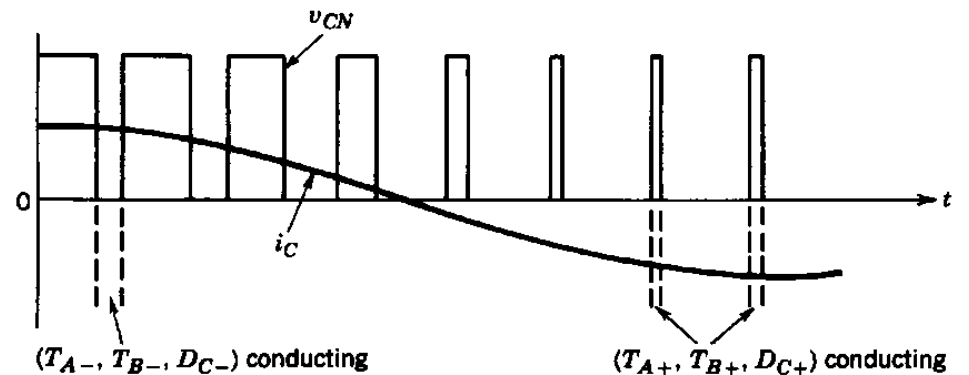
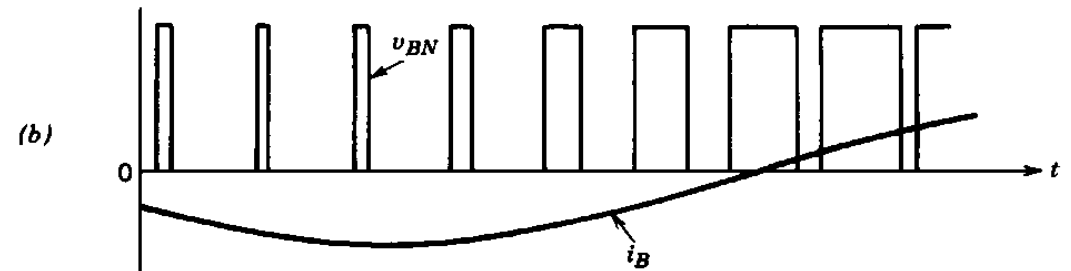
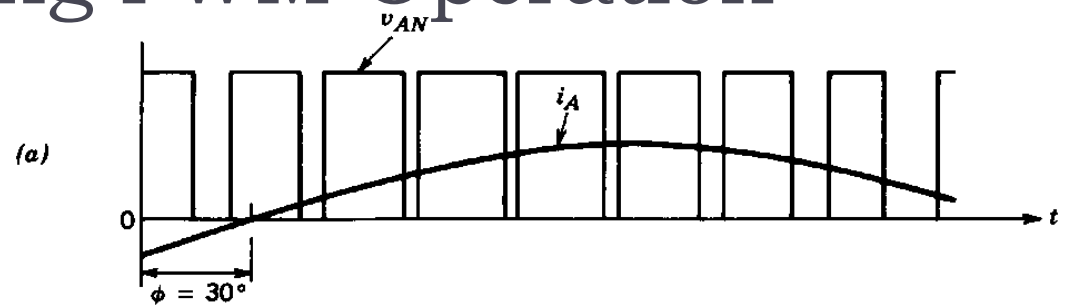


- ▶ The current consists of a dc component and the switching-frequency related harmonics

Device Conducting Square-Wave Operation

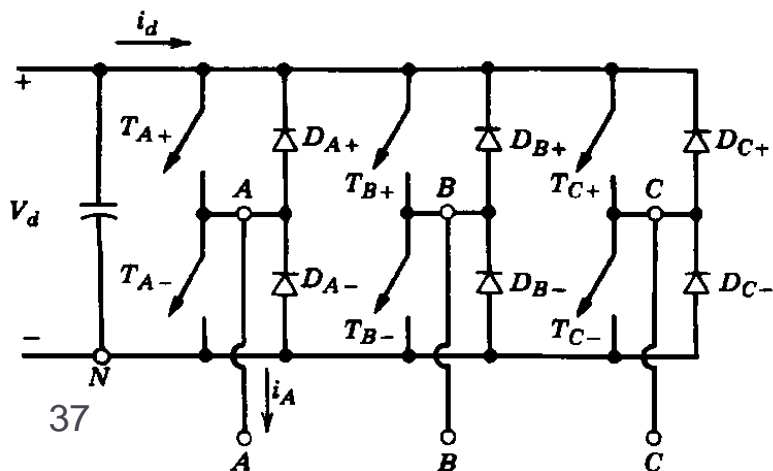


Device Conducting PWM Operation

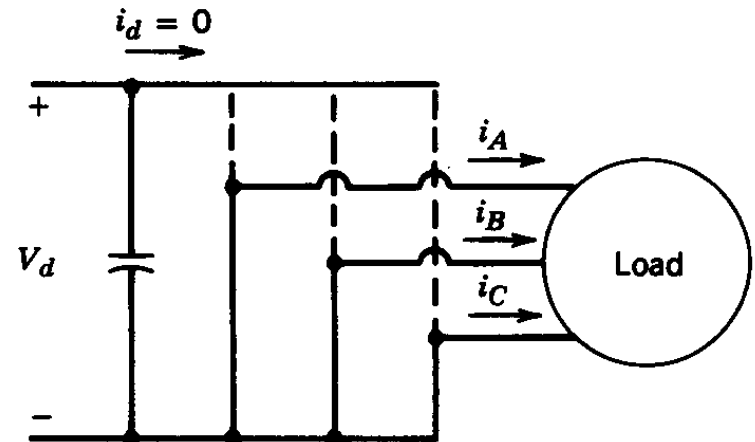
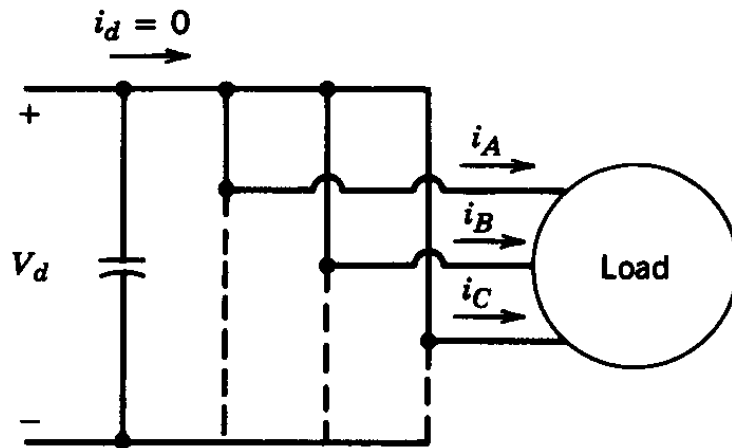


(T_{A-}, T_{B-}, D_{C-}) conducting

(T_{A+}, T_{B+}, D_{C+}) conducting

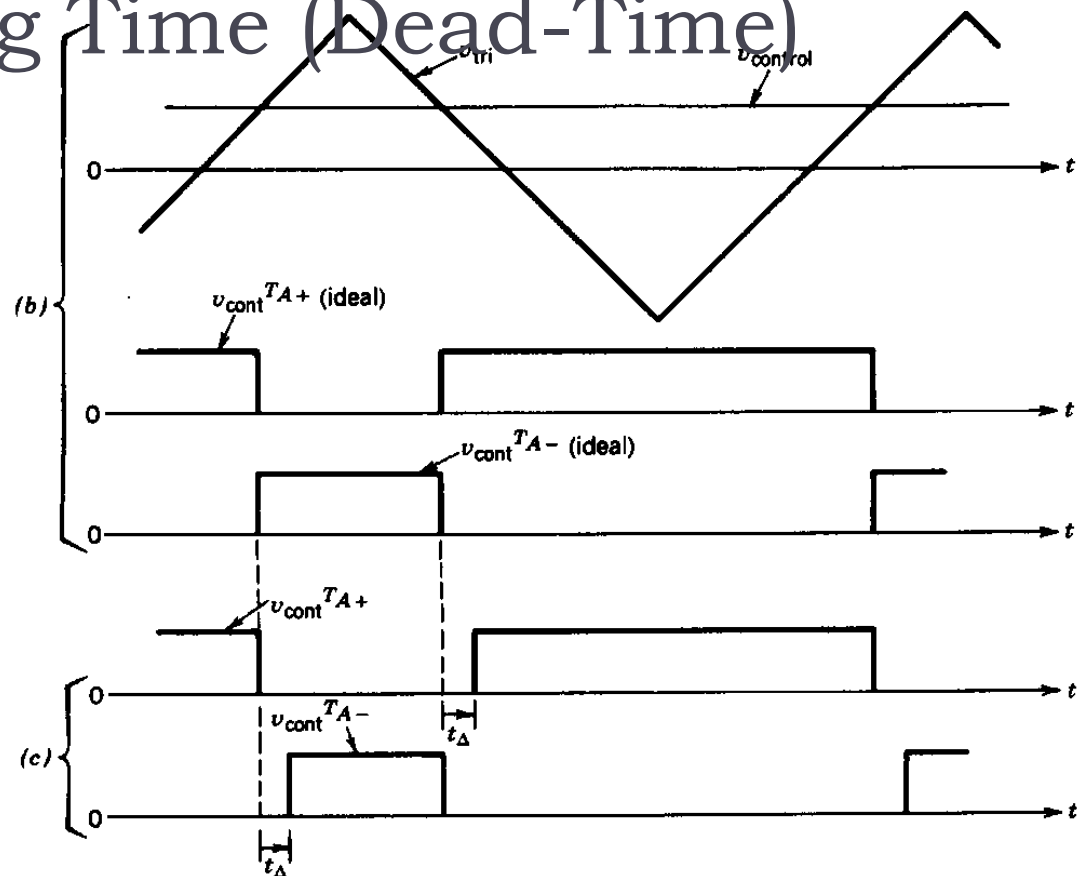
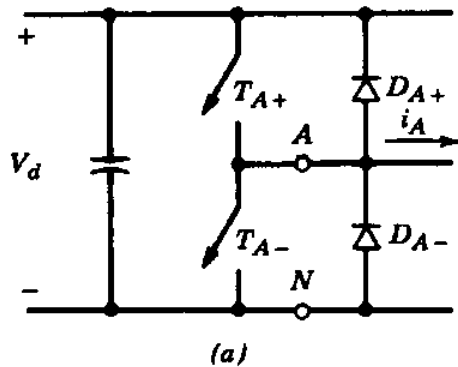


Short-Circuit States in PWM Operation

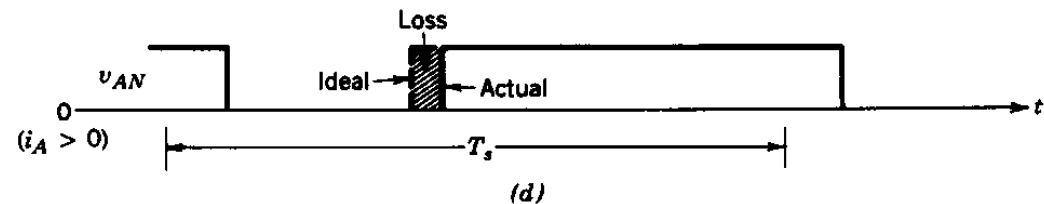


- ▶ top group or the bottom group results in short circuiting three terminals

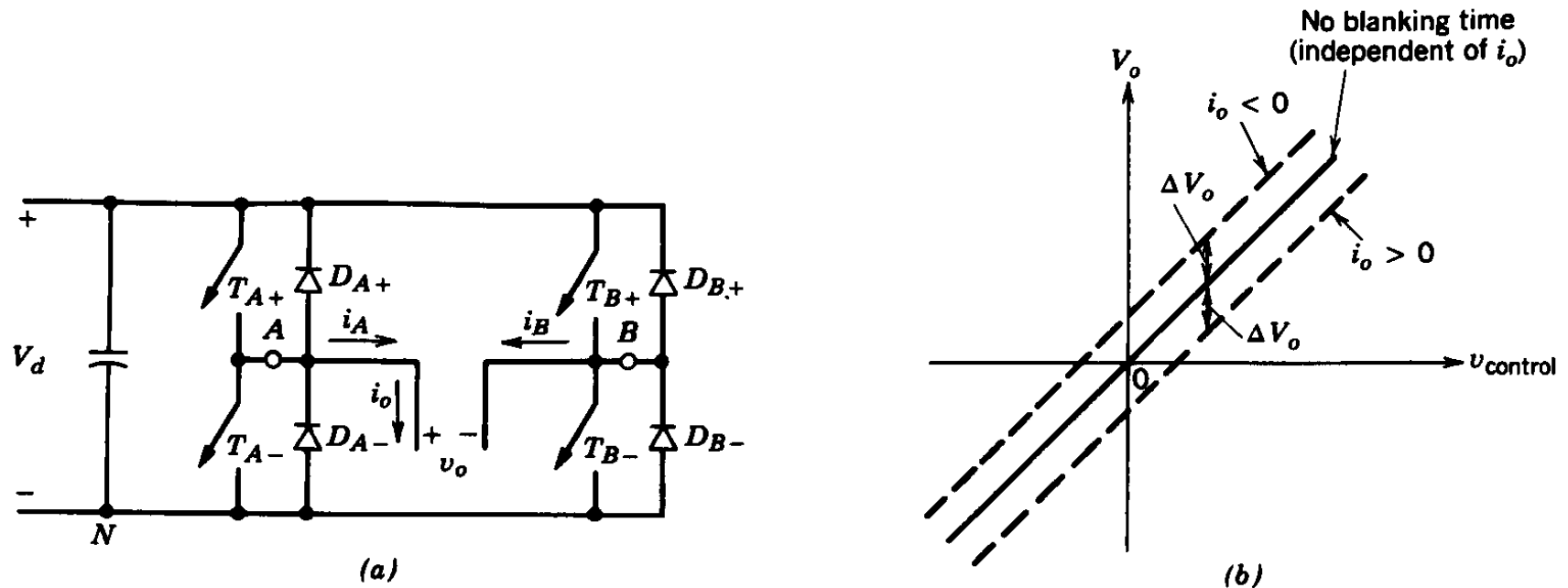
Effect of Blanking Time (Dead-Time)



- Results in nonlinearity



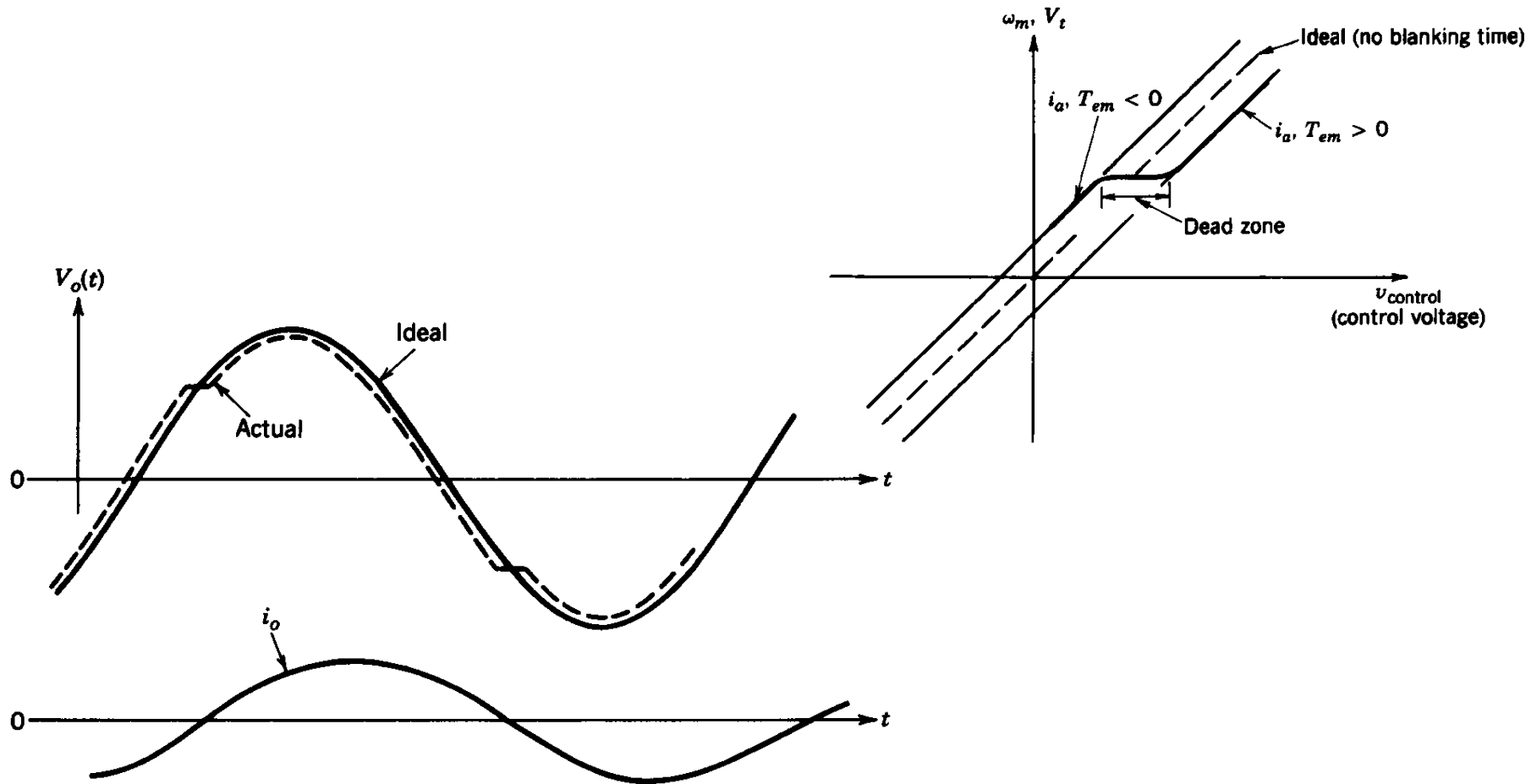
Effect of Blanking Time (Dead-Time)



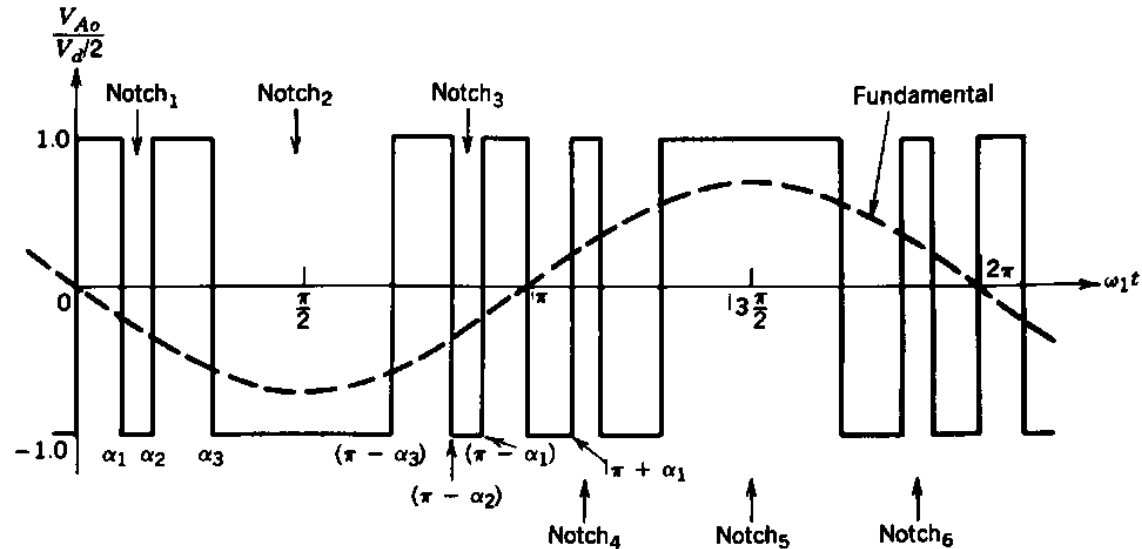
- ▶ Voltage jump when the current reverses direction

Effect of Blanking Time (Dead-Time)

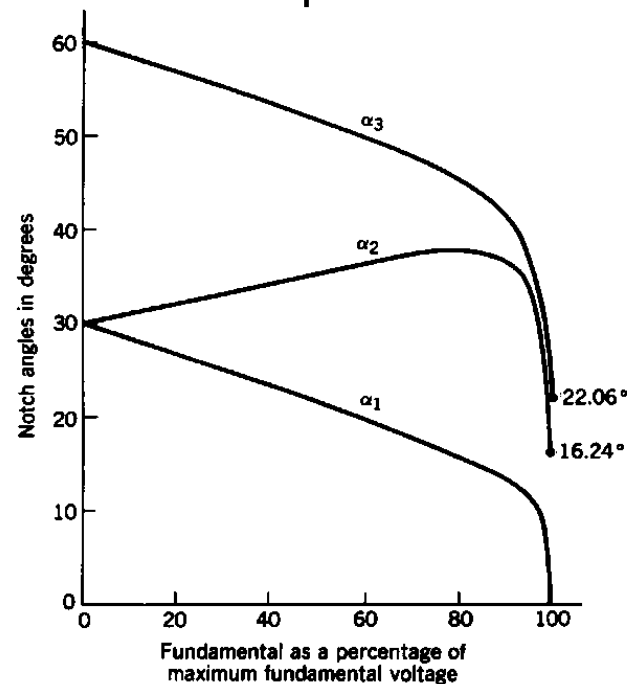
► Effect on the output voltage



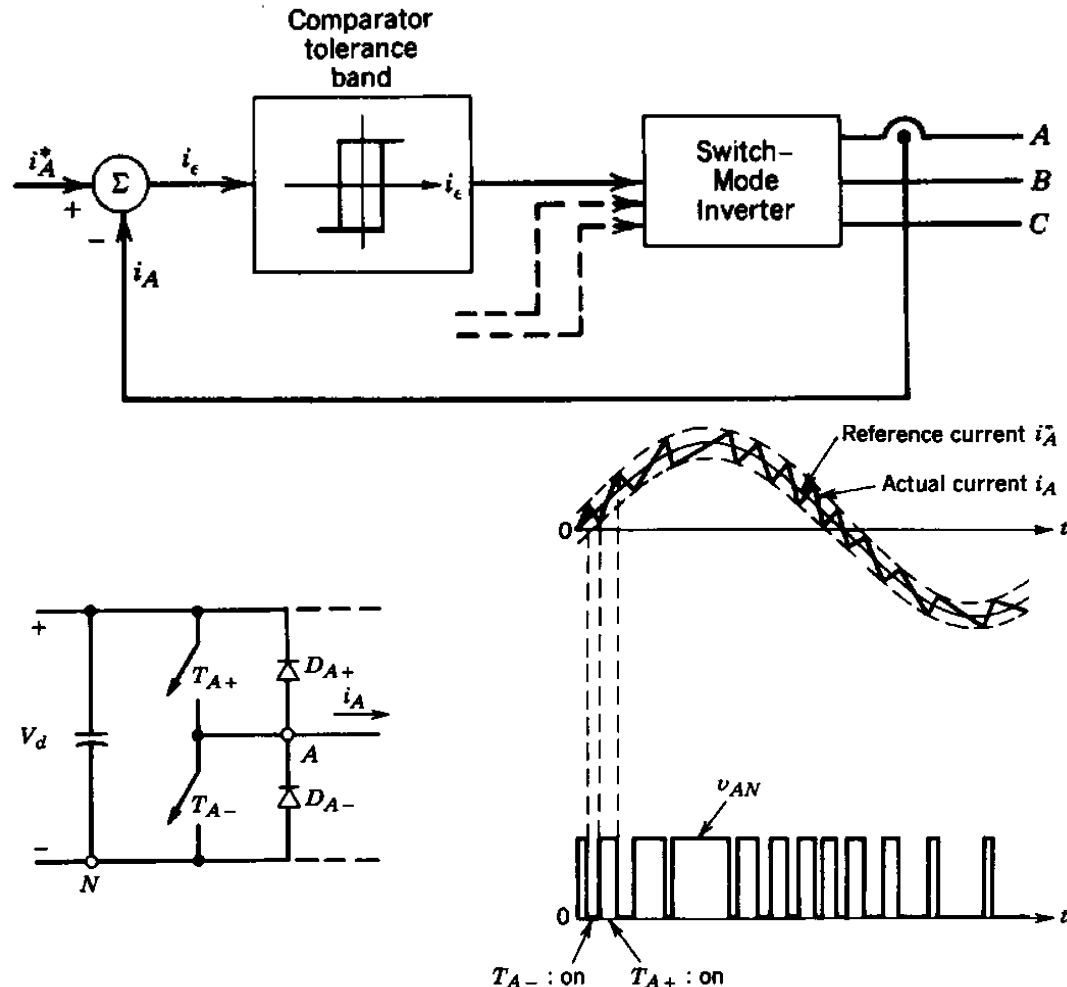
Programmed Harmonic Elimination



- Angles based on the desired output

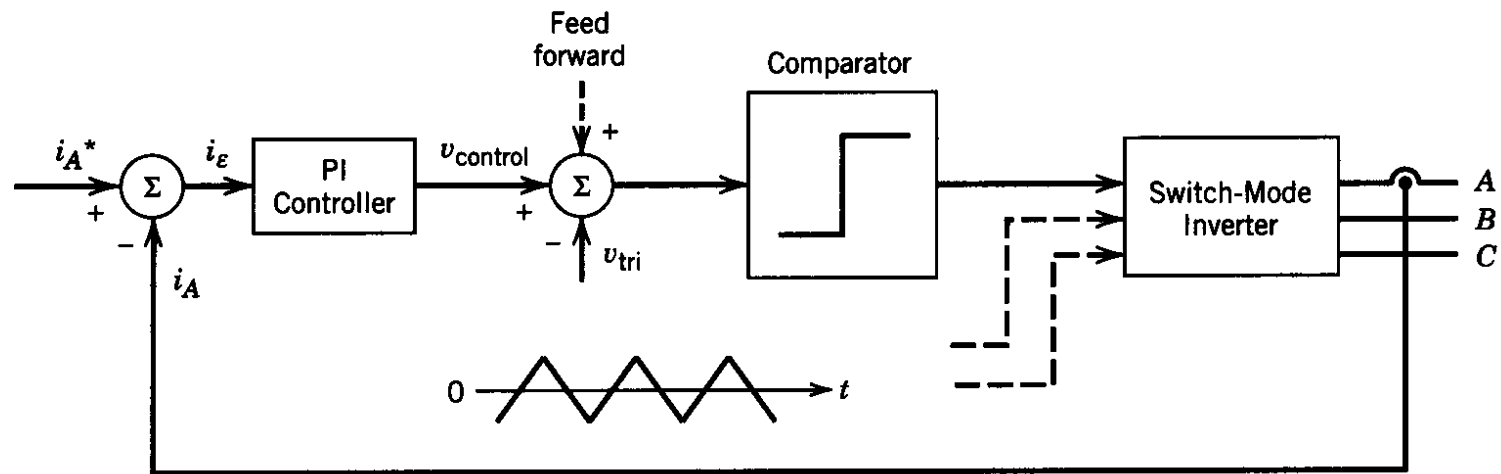


Tolerance-Band Current Control



- Results in a variable frequency operation

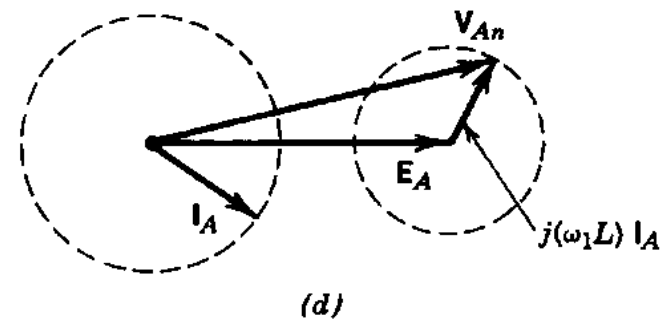
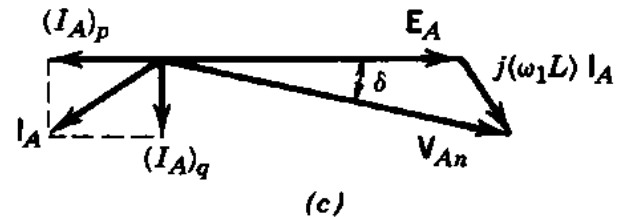
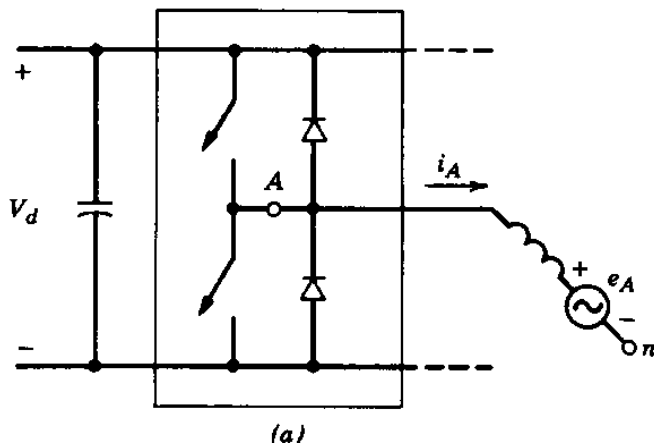
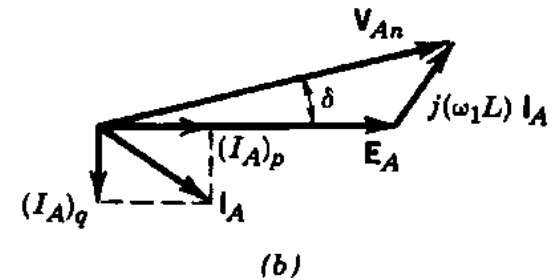
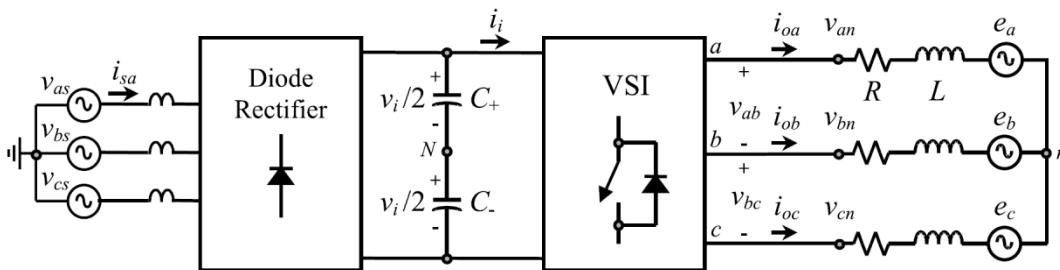
Fixed-Frequency Operation



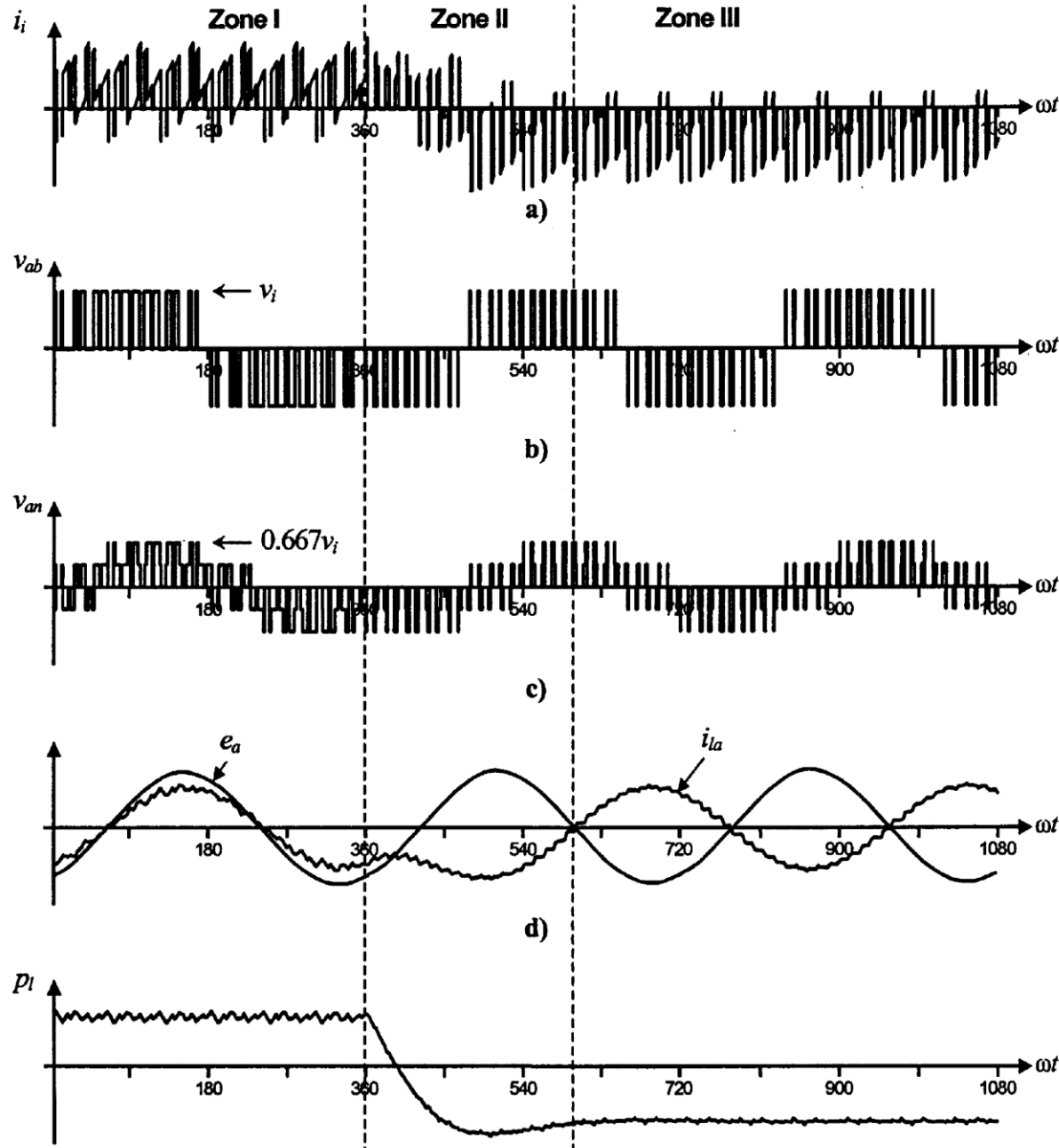
- ▶ Better control is possible using dq analysis!!!

Transition from Inverter to Rectifier Mode

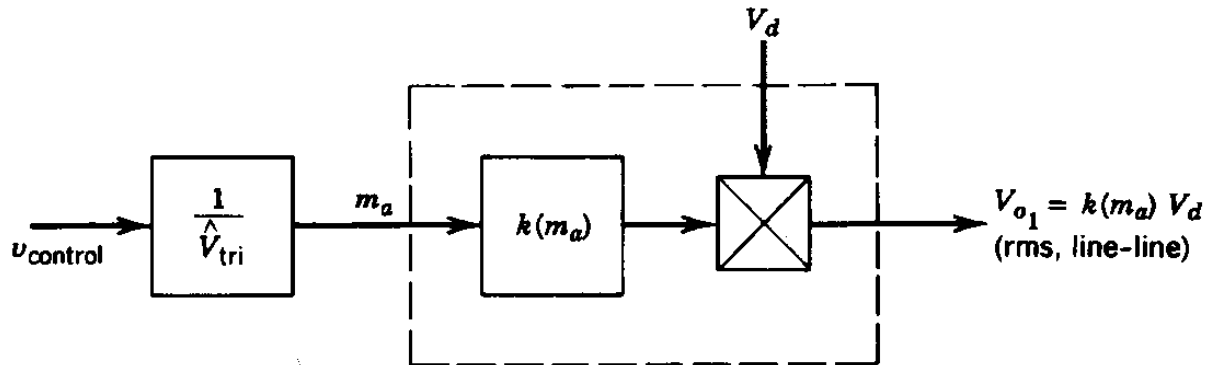
- Can analyze based on the fundamental-frequency



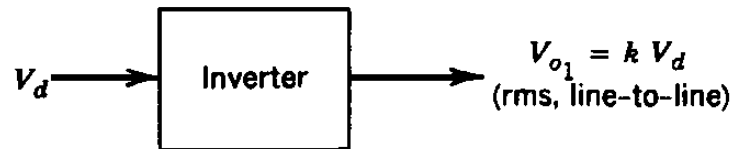
Transition from Inverter to Rectifier Mode



Functional representation in a block-diagram form of DC-AC Inverters

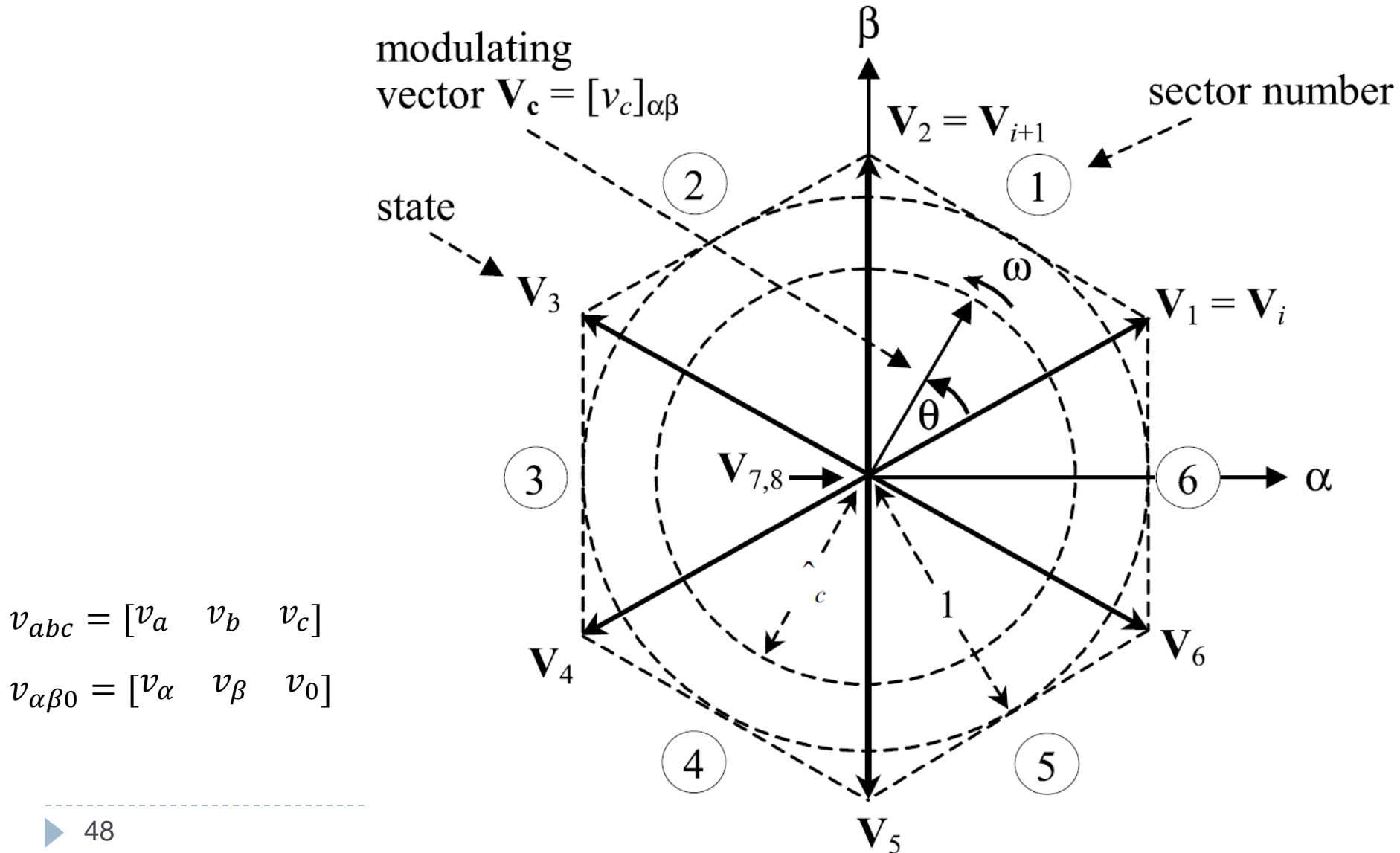


$$\text{for } m_a \leq 1.0 \quad \begin{aligned} k(m_a) &= 0.707 m_a && \text{1-phase} \\ &= 0.612 m_a && \text{3-phase} \end{aligned}$$

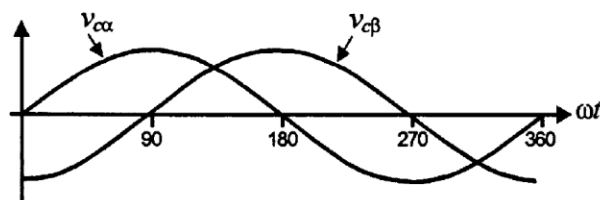
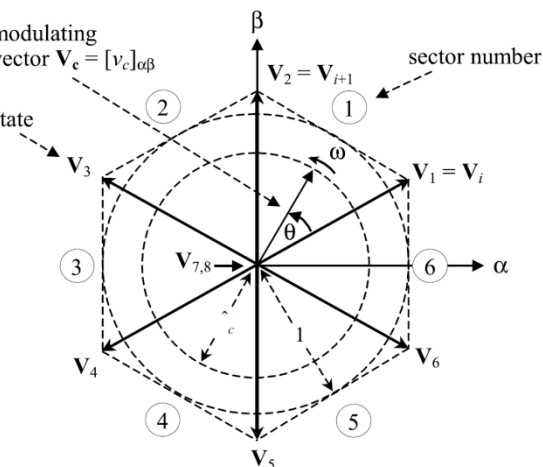
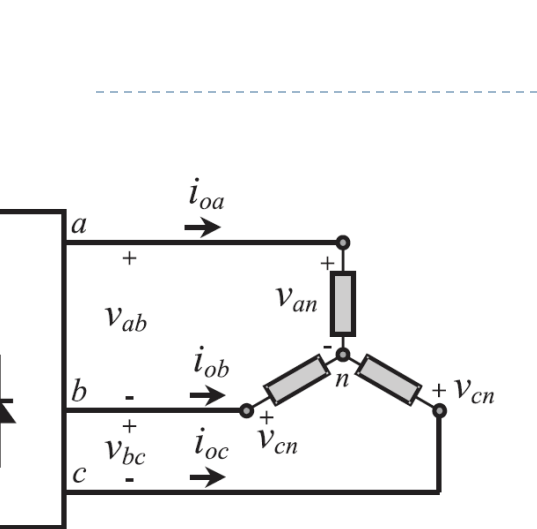


$$\begin{aligned} k &= 0.9 && \text{1-phase} \\ &= 0.78 && \text{3-phase} \end{aligned}$$

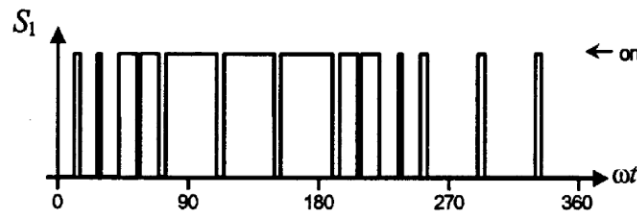
Space-Vector Transformation



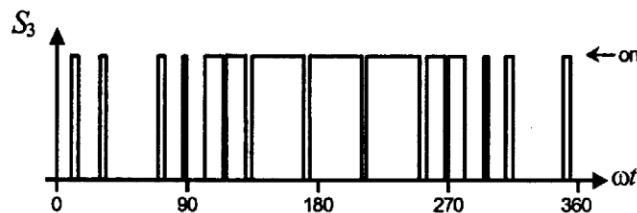
Space-Vector Modulation



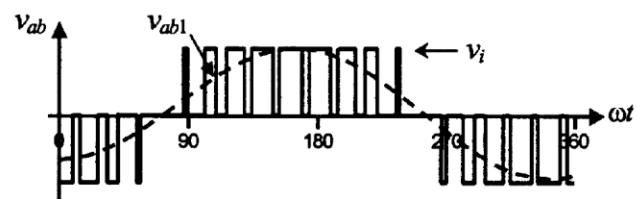
a)



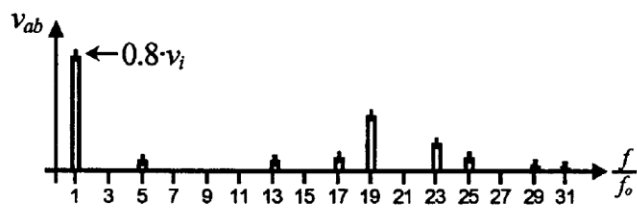
b)



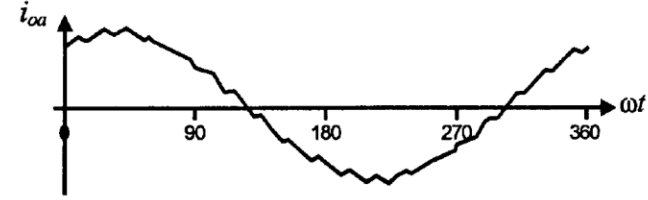
c)



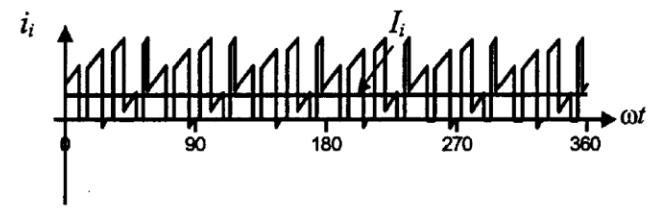
d)



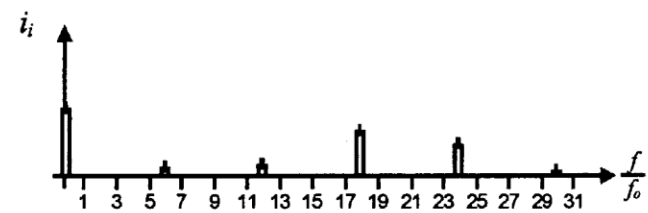
e)



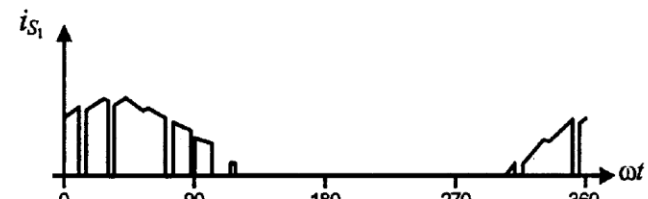
f)



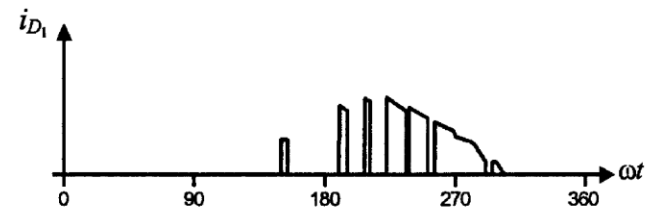
g)



h)



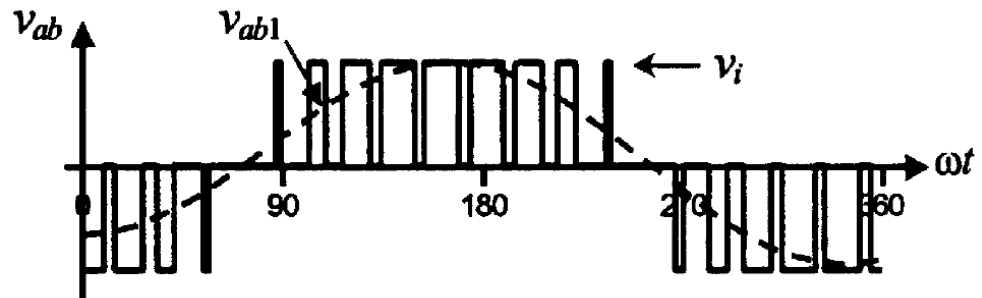
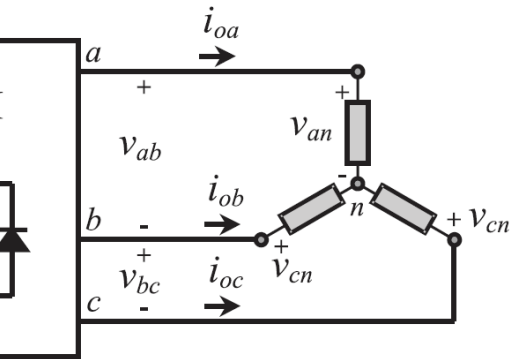
i)



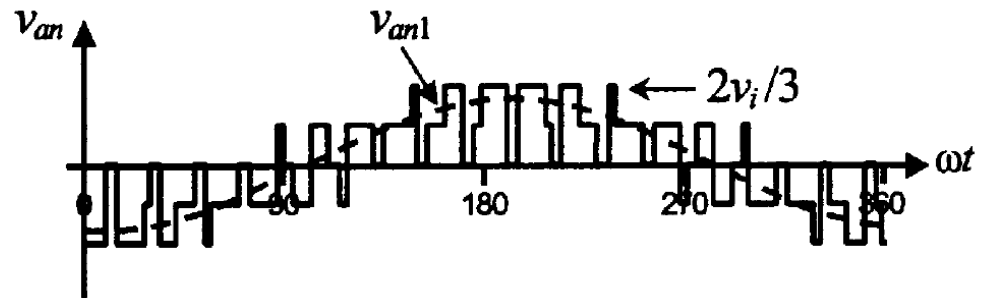
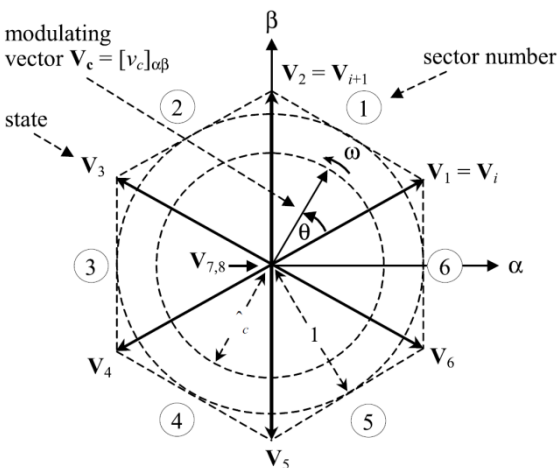
j)

Space-Vector Modulation

Phase Voltage

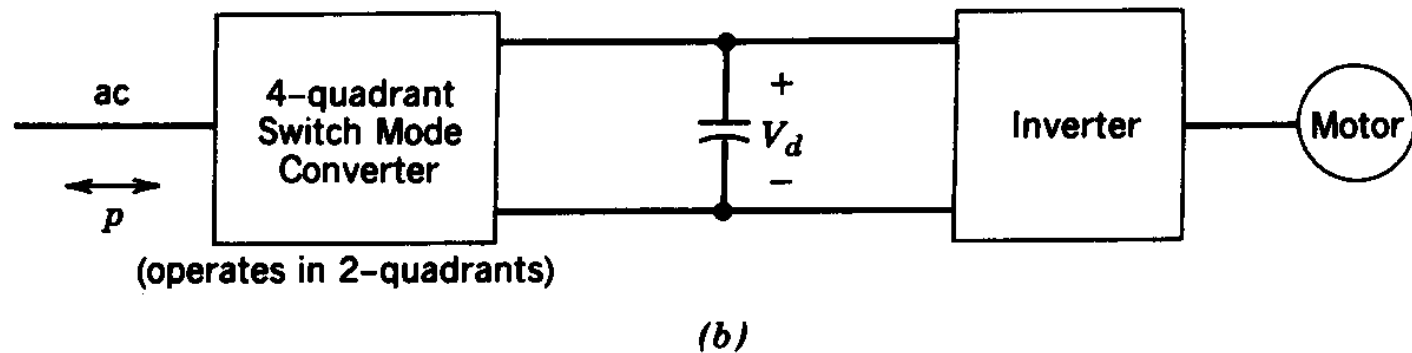
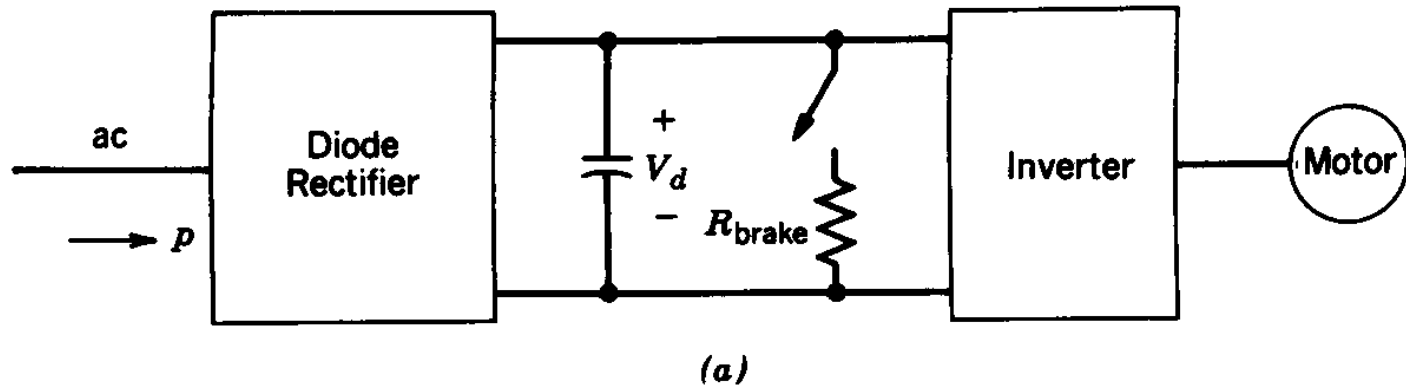


a)

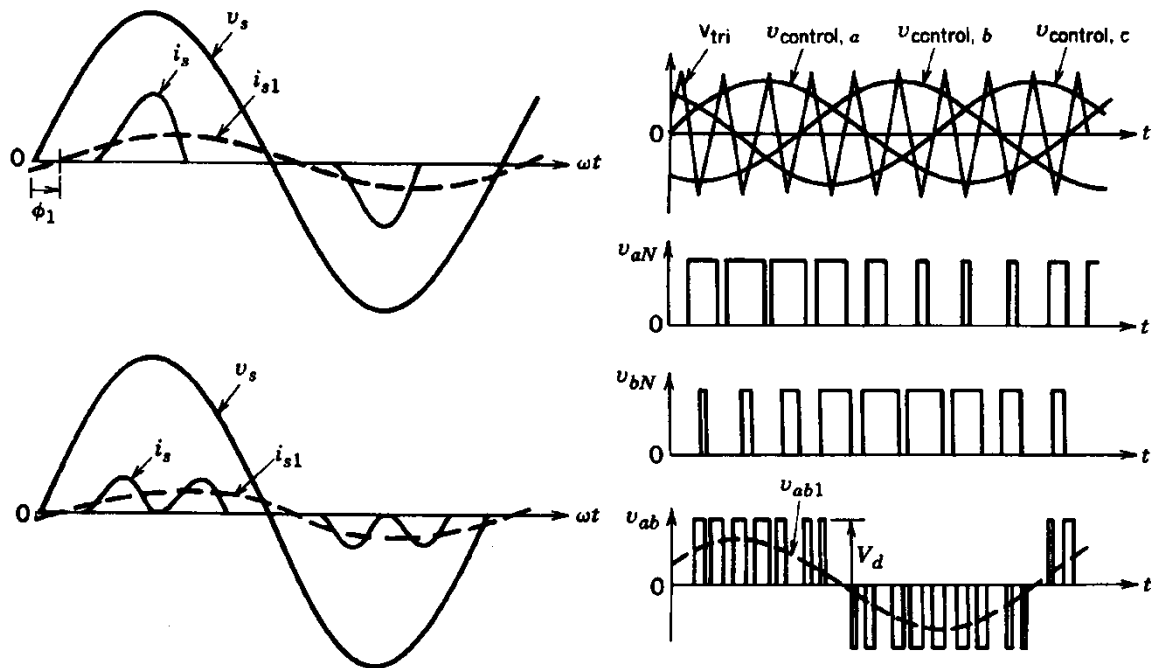
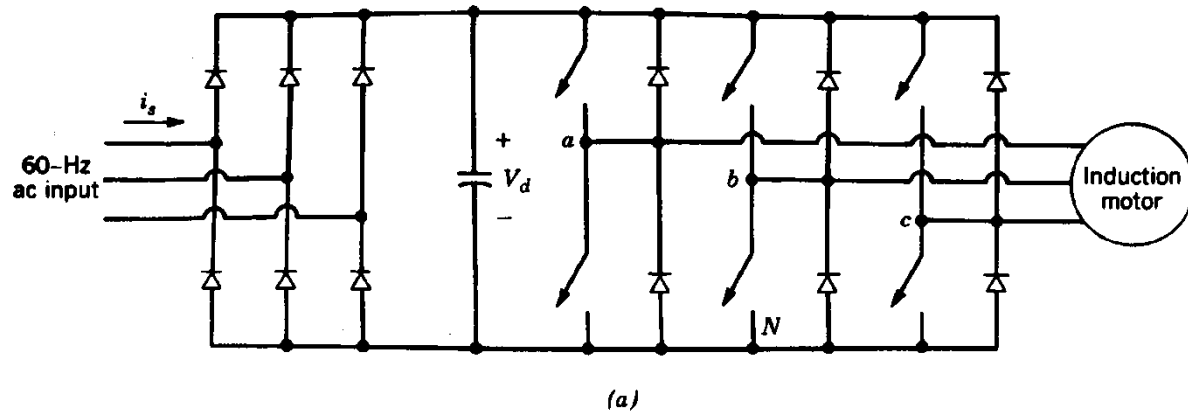


b)

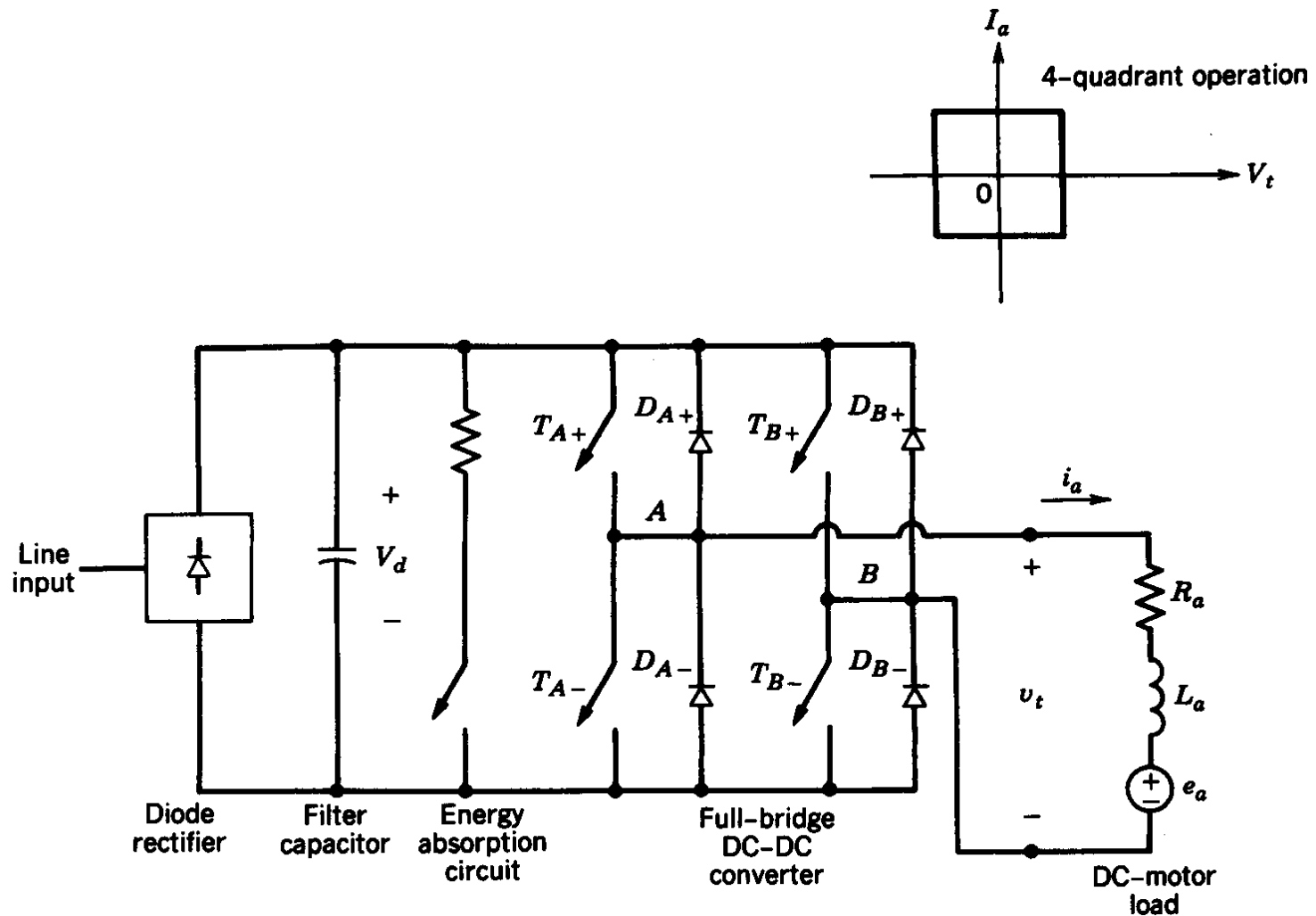
Recovered/Regenerative braking



Induction Motor Power Converter



DC motor drive



Homework
